

# Methodology for the Study of Dynamic ON-Resistance in High-Voltage GaN Field-Effect Transistors

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**Abstract**—We have developed a new methodology to investigate the dynamic ON-resistance ( $R_{ON}$ ) of high-voltage GaN field-effect transistors. The new technique allows the study of  $R_{ON}$  transients after a switching event over an arbitrary length of time. Using this technique, we have investigated dynamic  $R_{ON}$  transients in AlGaIn/GaN high-voltage, high electron-mobility transistors over a time span of ten decades under a variety of conditions. We find that right after an OFF-to-ON switching event,  $R_{ON}$  can be several times higher under dc conditions. The increase in  $R_{ON}$  is enhanced as the drain-source voltage in the OFF-state increases. The  $R_{ON}$  recovery process after an OFF-to-ON switching event is characterized by a fast release of trapped charge through a temperature-independent tunneling process followed by conventional thermally activated detrapping on a longer timescale. After a high-power-to-ON switching event, in contrast, detrapping only takes place through a temperature-independent process. We postulate that the fast temperature-independent detrapping originates from interface states at the AlGaIn barrier/AlN spacer interface. The thermally activated detrapping can arise from traps at the surface of the device or inside the AlGaIn barrier. These findings are relevant in the quest to engineer a reliable GaN power switch with minimum dynamic  $R_{ON}$  problems.

**Index Terms**—Border traps, current collapse, dynamic ON-resistance, FET, GaN, high electron-mobility transistor (HEMT), transient, trapping.

## I. INTRODUCTION

IN THE last few years, there has been a tremendous interest in the development of energy-efficient electrical power management systems. Recently GaN field-effect transistors have emerged as a disruptive technology with great potential for improved power switching performance. This arises from the outstanding material properties of GaN [1]. A better than three orders of magnitude improvement in ON-resistance/breakdown-voltage tradeoff is projected to be achievable with GaN FETs over current Si-based power-switching technology [2].

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Among several technical requirements on an efficient power switch, a critical one is obtaining a very low ON resistance ( $R_{ON}$ ) immediately after switching from a high-voltage OFF state to a low-voltage ON state. In more mature RF power GaN high electron-mobility transistors (HEMTs), dynamic switching problems, such as current collapse, gate lag, and drain lag, are often present and detract from RF power performance [3], [4]. In power switching applications, these same issues manifest themselves as a dynamic  $R_{ON}$  in which after an OFF-ON switching event,  $R_{ON}$  remains high for a period of time [5], [6]. To date, there has been little research on this important issue [7], [8].

Toward the goal of achieving fundamental understanding of this problem, we have developed a new dynamic  $R_{ON}$  transient measurement methodology which allows the observation of  $R_{ON}$  transients after a switching event over a time period that can span many decades. This technique combines the measurements of two different instruments. The acquired dynamic ON-resistance transients are then analyzed using a current-transient methodology recently developed [9].

We demonstrate the usefulness of this approach by carry out a systematic study of dynamic  $R_{ON}$  on high-voltage GaN-HEMTs on SiC substrate as a function of time, temperature, and pulse conditions. In the samples that we have investigated, we find that after biasing at an OFF-state voltage, the initial value of  $R_{ON}$  increases as the voltage increases. Also, on a short timescale, we find that  $R_{ON}$  recovers in a temperature-independent manner. In contrast, on a longer timescale, the  $R_{ON}$  transients are found to be thermally activated.

We propose that the fast recovery behavior takes place through an electron-tunneling process from traps located inside the AlGaIn barrier close to the GaN channel layer. Likely candidates are interface states at the AlN spacer/AlGaIn barrier interface. The slower thermally activated recovery is attributed to traps in the AlGaIn or at the surface.

This paper provides a methodology toward understanding and mitigating dynamic  $R_{ON}$  issues in high-voltage GaN FETs. This paper presents an augmented version of a recent conference presentation [10]. It is organized as follows. Section II explains the measurement technique. Section III briefly describes the devices used to illustrate the technique and presents detailed results obtained under different conditions. Section IV illustrates the importance of epitaxial growth details on dynamic  $R_{ON}$ . Lastly, Section V hypothesizes the physical origin of the trapping behavior that is observed.

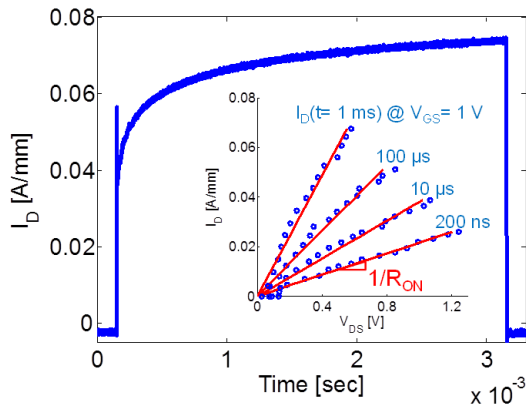


Fig. 1.  $I_D$  waveform measured by pulsed  $I$ - $V$  system. The device is synchronously switched from an OFF-state quiescent bias of  $V_{GSQ} = -10$  V,  $V_{DSQ} = 50$  V to an ON-state of  $V_{GS} = 1$  V and  $V_{DS}$  changing from 50 mV to 1.2 V at ambient temperature of 25 °C. Through the simultaneous measurement of both  $I_D(t)$  and  $V_{DS}(t)$  transients in the linear regime, the instantaneous  $R_{ON}$  (200 ns  $\leq t \leq 3$  ms) is extracted as shown in the inset.

## II. DYNAMIC $R_{ON}$ MEASUREMENT TECHNIQUE

The dynamic  $R_{ON}$  measurement technique that we have developed is capable of collecting  $R_{ON}$  transients from 200 ns to any arbitrary length of time. For this, we use two different instruments: an Auriga AU4750 pulsed  $I$ - $V$  system for  $R_{ON}$  transients from 200 ns to 3 ms and an Agilent B1500A semiconductor device analyzer (SDA) for  $R_{ON}$  transients beyond 3 ms. In both the cases, synchronous switching of  $V_{GS}$  and  $V_{DS}$  is performed.

With the pulsed  $I$ - $V$  system, we successively switch from an OFF-state quiescent ( $Q$ ) bias to an ON state given by  $V_{GS} = 1$  V and several  $V_{DS}$  values in the linear regime of device operation ( $\leq 1.2$  V). In this manner, we measure the linear drain current characteristics close to the origin. Fig. 1 shows a typical measured  $I_D$  waveform in a high-voltage GaN HEMT after it is switched from an OFF state ( $V_{GSQ} = -10$  V,  $V_{DSQ} = 50$  V) to ON state.  $I_D(t)$  and  $V_{DS}(t)$  are measured every 200 ns within a pulse width of 3 ms and a duty cycle of 10%. For each data point, the measurement time is 5 ns. To minimize noise and enhance measurement accuracy, each extracted data point represents an average of 300 measurements. As a result of heavy electron trapping that occurs during the OFF-state period, ON-state  $I_D$  in the linear regime shows a very slow increase in time toward the expected dc value. In addition, because the pulsed  $I$ - $V$  system itself has an internal source resistance, as the device  $R_{ON}$  decreases, the range of  $V_{DS}$  values in the ON state decreases accordingly. Through the simultaneous measurement of both  $I_D(t)$  and  $V_{DS}(t)$  transients in the linear regime (Fig. 1, inset), the instantaneous  $R_{ON}$  (200 ns  $\leq t \leq 3$  ms) can be extracted.

$R_{ON}$  transients for longer time periods can be explored using SDA. The synchronous pulsed mode of B1500A allows the continuous measurement of  $R_{ON}$  transient from 3 ms to any arbitrary time. In contrast to the pulsed  $I$ - $V$  system, B1500A can measure  $I_D(t)$  transients at a constant  $V_{DS}$  value (0.5 V has been used here). By adjusting the time that the device resides in the OFF state, one can closely match the beginning of transient as measured by SDA with the end point of the

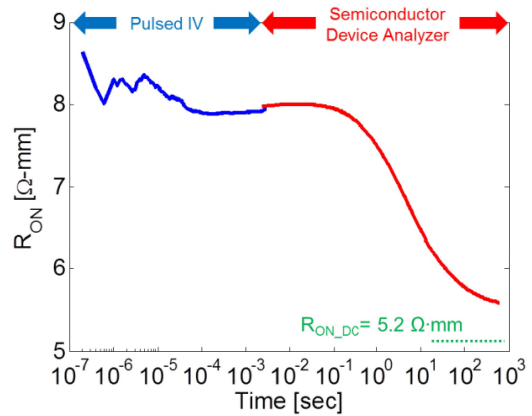


Fig. 2.  $R_{ON}$  transients from 200 ns to 1000 s on GaN-on-SiC high-voltage HEMTs from an OFF state ( $V_{GSQ} = -5$  V,  $V_{DSQ} = 40$  V) to ON-state switching at ambient temperature of 55 °C. Blue line is obtained from pulsed  $I$ - $V$  system (Auriga AU4750) and red line from SDA (Agilent B1500A). Also shown are the dc values of  $R_{ON}$  obtained after fully detrapping the device (marked as  $R_{ON\_DC}$ ). This shows 66% higher  $R_{ON}$  at 200 ns than in dc.

transient measurement obtained by the pulsed  $I$ - $V$  system and obtain a complete transient that spans many decades of time. One example is shown in Fig. 2 for the transients obtained over ten decades. The blue line is measured from the pulsed  $I$ - $V$  system and the red one comes from SDA. Also shown are the DC values of  $R_{ON}$  obtained after fully detrapping the device under visible light illumination.

In these synchronous pulsed measurements using the pulsed  $I$ - $V$  system and SDA, fast switching of  $V_{GS}$  and  $V_{DS}$  is important so as to prevent the occurrence of a momentary high-power state during the transition (hard switching). Fig. 3 shows the waveforms of three different switching events from the OFF state ( $V_{GSQ} = -5$  V,  $V_{DSQ} = 40$  V) to the ON state in one of the test samples. These measurements are obtained through the pulsed  $I$ - $V$  system. In one event, the pulsing of  $V_{DS}$  and  $V_{GS}$  is synchronous. In the other two events, a delay of 200 or 400 ns is introduced between the switching-off of  $V_{DS}$  and the switching-on of  $V_{GS}$ . The corresponding  $R_{ON}$  transient measurements are shown as follows.

The time lapse between the samples in the waveforms at the top of Fig. 3 is 5 ns. With our relatively small-size devices, when tested through the pulsed  $I$ - $V$  system, a fast slew rate of 1 V/ns is measured. In the synchronous case, this results in a very short overlap (a few nanoseconds) of  $V_{DS}$  and  $V_{GS}$  waveforms at relatively low values of  $V_{DS}$ . This does not introduce any visible trapping in the device as evidenced by the resulting  $R_{ON}$  transients which are essentially identical to those obtained when a delay of 200 or 400 ns is introduced between the two pulses. The situation might be different in the case of large-size devices where the slew rate can be significantly slower and an adjustment of delay time between  $V_{DS}$  and  $V_{GS}$  pulses might be needed.

In the synchronous pulse mode of B1500A, there is no way to control the relative delay between the gate and drain pulses. However, because the switching occurs on a much slower time scale and we always observe a good match of characteristics at the boundary with the data acquired from the pulsed  $I$ - $V$

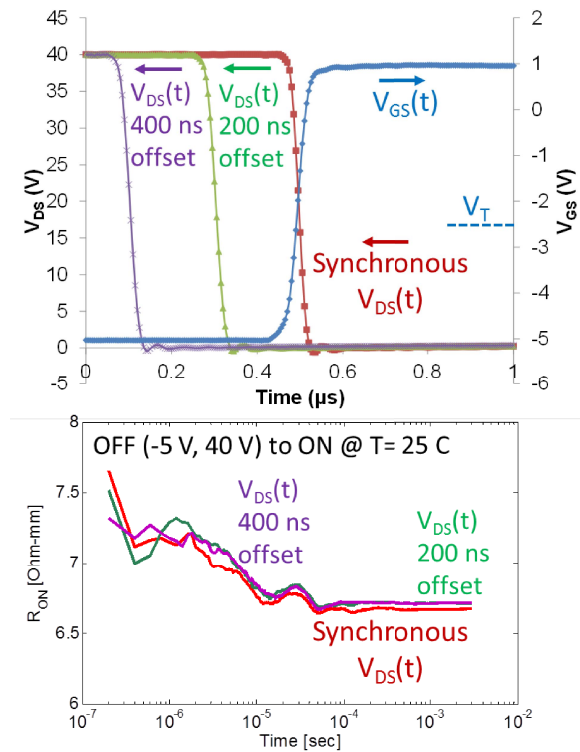


Fig. 3. Top:  $V_{DS}$  and  $V_{GS}$  waveforms of three switching events from an OFF state ( $V_{GSQ} = -5$  V,  $V_{DSQ} = 40$  V) to ON state. In one event, the pulsing is synchronous. In the other two, a delay of 200 ns or 400 ns is introduced between the falling edge of  $V_{DS}$  and the rising edge of  $V_{GS}$ . Bottom: resulting  $R_{ON}$  transients are unaffected by the relative alignment of  $V_{DS}$  and  $V_{GS}$  pulses, indicating that trapping during the transient is negligible. In our relatively small size devices, a fast slew rate of 1 V/ns is obtained.

system, we conclude that any hard switching that might occur results in negligible trapping on the time scale in which we use this tool ( $t > 3$  ms).

The stitching approach shown in Fig. 2 is time-consuming and inevitably leaves a small residual discrepancy between the measurements obtained through the two techniques at 3 ms stitching point. This can cause noise in the final time constant spectra [9]. We have eliminated this problem by appropriately scaling the transient data obtained from SDA. Fig. 4 shows how this scaling works. We show here  $R_{ON}$  transients obtained with the pulsed  $I-V$  system, as specified earlier, and SDA. Both sets of transients are obtained with the device at the same OFF-state bias point. Before SDA measurements, the device is kept in the OFF state for 50, 75, or 100 s. All of them result in a visible mismatch with the pulsed IV data. As the OFF-state time increases, the initial value of  $R_{ON}$  at 3 ms increases because of higher electron trapping. The evolution of transient beyond that initial point, however, is independent of this initial value. This can be seen in the inset of Fig. 4 that graphs  $[R_{ON}(t) - R_{ON,DC}] / [R_{ON}(t = 3 \text{ ms}) - R_{ON,DC}]$  for the three cases. As seen, the transients closely overlap each other. This suggests that the  $R_{ON}$  transients are largely independent of the initial value of  $R_{ON}$  at 3 ms and that simple scaling can be used to stitch the  $R_{ON}$  measurements obtained from SDA to those derived from pulsed  $I-V$  system.

From this paper, we have synthesized the following approach to obtain complete  $R_{ON}$  transients. First, an  $R_{ON}$

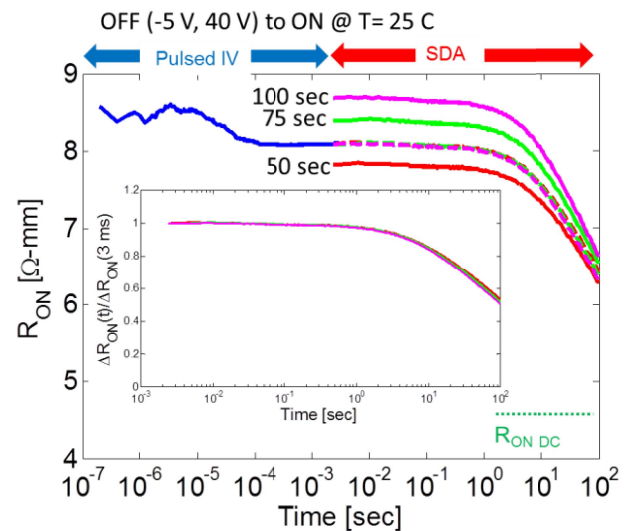


Fig. 4.  $R_{ON}$  transients in OFF ( $V_{GSQ} = -5$  V,  $V_{DSQ} = 40$  V) to ON-state switching from pulsed  $I-V$  in the blue line and from SDA using different OFF-state times of 50, 75, or 100 s. A visible mismatch occurs with the pulsed IV data. Scaling the SDA-obtained data to match  $\Delta R_{ON}(t)/\Delta R_{ON}(3 \text{ ms})$  makes all lines overlap with each other as shown in dotted line. Inset: identical normalized  $R_{ON}$  recovery rates suggesting that the  $R_{ON}$  transients are largely independent of the initial value of  $R_{ON}$  (3 ms).

transient is obtained using the pulsed  $I-V$  system. Then, the OFF-state time in the B1500A is controlled to produce an  $R_{ON}$  transient that closely matches the final value obtained from the pulsed  $I-V$  system. The residual mismatch is resolved through scaling of B1500A data set to match with the pulsed IV data at  $t = 3$  ms. The overall transient is then analyzed using the time constant spectrum approach of [9].

### III. DYNAMIC $R_{ON}$ IN HIGH-VOLTAGE GaN HEMTs ON SiC

We have demonstrated the usefulness of our proposed dynamic  $R_{ON}$  technique by studying in detail industrially prototyped AlGaIn/GaN HEMTs grown by metal organic chemical vapor deposition on SiC for S-band power amplifier application. The heterostructure includes a GaN cap and an AlN spacer. The device design features an integrated field plate and a source-connected field plate. The gate width is  $6 \times 100 \mu\text{m}$ . The devices are depletion mode with a threshold voltage  $\sim -3$  V. The breakdown voltage of devices is  $\sim 160$  V. All the measurements are performed in dark and in air. There was no discernible permanent degradation of devices as a result of repeated testing under the conditions used in this paper.

Fig. 2 shows  $R_{ON}$  transients from representative devices when the device is switched from an OFF state with  $V_{GSQ} = -5$  V and  $V_{DSQ} = 40$  V at  $T = 55$  °C.  $R_{ON}$  at 200 ns is  $\sim 66\%$  higher than in dc ( $R_{ON,DC}$ ). Such a high dynamic  $R_{ON}$  represents a big problem for power-switching applications. The pattern of recovery of  $R_{ON}$  exhibits a very slow transient in the s-ks time range.

To gain insight into the physics of this dynamic behavior, we have carried out OFF to ON transients from different quiescent  $V_{DS}$  values at ambient temperature, as shown in Fig. 5.

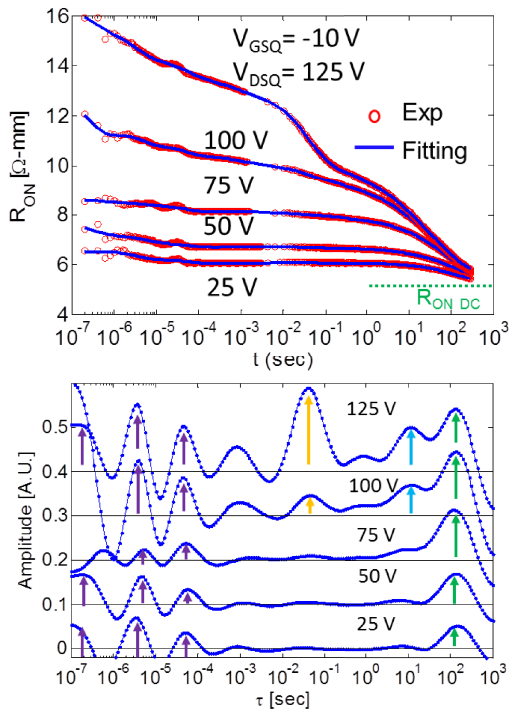


Fig. 5. Top: dynamic  $R_{ON}$  transients after OFF-to-ON switching events from different quiescent  $V_{DS}$  conditions from  $V_{DSQ} = 25$  V to 125 V in 25 V increments at ambient temperature of 25 °C. Red dots are measurements and blues lines are fitting curves through a sum of exponential terms with time constants ranging from  $10^{-7}$  to  $10^3$  s as shown in the bottom. The device exhibits prominent time constants in the 1–1000 s range and some in the submicrosecond to millisecond range. As  $V_{OFF}$  increases, the dynamic  $R_{ON}$  also increases, but the time constants do not change.

As  $V_{DSQ}$  increases, the dynamic  $R_{ON}$  increases in a prominent manner presumably as a result of increased extension of high-field region into the drain.

The dominant time constants underlying these transients can be obtained using a time constant spectrum analysis [9]. We use a sum of exponentials with 20 time constants per decade within the range from  $10^{-7}$  to  $10^3$  s. Examples of fits are shown at the top of Fig. 5 and the resulting time constant spectra are shown on the bottom of this figure. These indicate that there are multiple time constants with values that do not change as the applied electric field in the OFF state increases. Only the magnitude of the signals are affected by increasing  $V_{DSQ}$ . In particular, there are two prominent time constants in the 10–1000 s range and some more in the submicrosecond to millisecond range. All get more prominent as  $V_{DSQ}$  increases. There is also a time constant  $\sim 50$  ms that prominently increases when  $V_{DSQ} > 100$  V. This could be because of the depletion region sweeping through a particular defect at higher values of  $V_{DSQ}$ .

To further understand the physical processes behind these transients, we have performed dynamic  $R_{ON}$  measurements at different ambient temperatures and their time constant spectra have been derived as presented in Fig. 6. In this figure, the dominant transients substantially speed up as the temperature increases. The time constant spectra at different temperatures show this acceleration very clearly. Dynamic  $R_{ON}$  at 200 ns shows slightly negative dependence as the

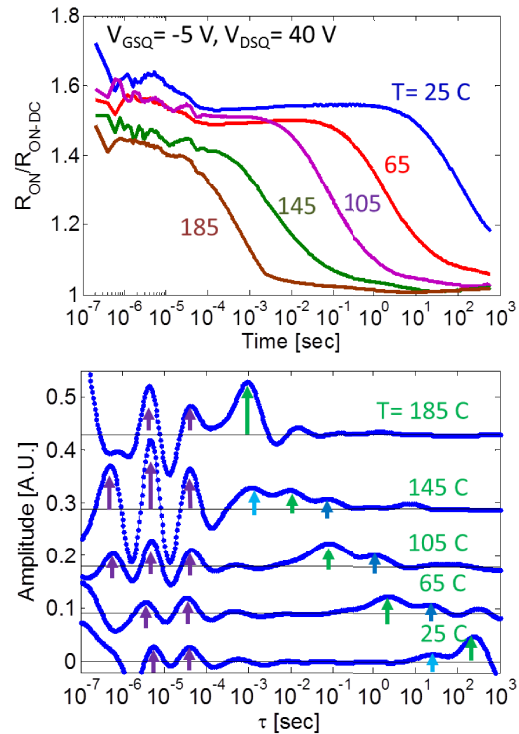


Fig. 6. Top:  $R_{ON}/R_{ON,DC}$  transients at different ambient temperatures for  $V_{GSQ} = -5$  V and  $V_{DSQ} = 40$  V. The resulting time constant spectra (bottom) clearly indicate that the dominant transients for long time substantially speed up as the temperature increases, whereas short time constants are independent of temperature.

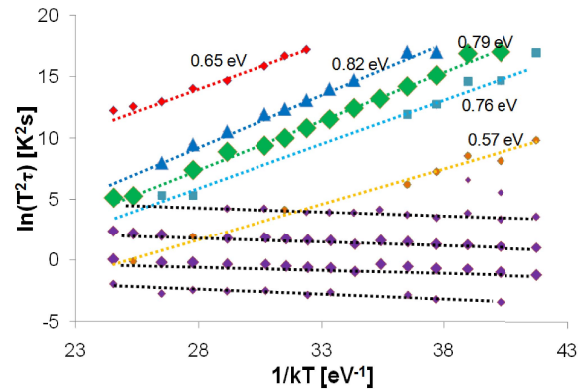


Fig. 7. Arrhenius plot of time constant spectrum of Fig. 6. The size of the symbols is proportional to the height of time constant peak. Dominant traps at 0.79, 0.82, and 0.76 eV are identified. A set of short time constants, which are independent of temperature, are also observed. They are responsible for fast transients.

temperature increases. This is most likely because of the high voltage trapping process resulting in less trapping as the temperature increases because in the OFF state, there is always a counterbalancing detrapping process that is enhanced. In addition to this, the device also exhibits fast transients that change less with temperature. This temperature-independent behavior for short times is also verified in the corresponding spectra.

Following the methodology of [9], we have plotted the evolution of dominant time constants with temperature in an Arrhenius plot (Fig. 7). The size of the symbols in this figure is

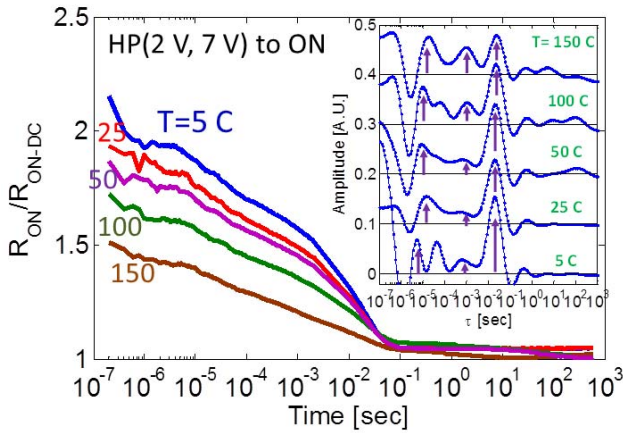


Fig. 8. High power to ON-state transients at different ambient temperatures and the resulting time constant spectra (inset). The high-power-state bias is  $V_{GSQ} = 2$  V and  $V_{DSQ} = 7$  V (the power level was 5.4 W/mm at ambient temperature of 25 °C corresponding to the red line). The transients are dominated by temperature-independent fast time constants. No thermally activated slow-transients are observed.

proportional to the height of the time constant peaks. From this Arrhenius plot, two distinct patterns emerge: a set of long time constants with thermally activated behavior and another set of short time constants that are independent of temperature. The long thermally activated time constants can be associated with conventional traps. The dominant traps are estimated at 0.79, 0.82, and 0.76 eV below the conduction band edge. Traps at similar energies have been reported by other authors in similar structures [11]–[13].

To further clarify the physics, we have also performed high power (HP) to ON transients. Fig. 8 shows the dynamic  $R_{ON}$  transients from a quiescent bias of  $V_{GS} = 2$  V,  $V_{DS} = 7$  V, and their respective time constant spectra at different ambient temperatures. The power level was 5.4 W/mm at ambient temperature of 25 °C corresponding to the red line. The transients are dominated by fast time constants only. In contrast to the data in Figs. 5 and 6, there are no slow thermally activated transients present. Furthermore, the dominant time constants of transients in Fig. 8 are temperature-independent as the spectrum clearly reveals. The initial value of  $R_{ON}/R_{ON,DC}$  at 200 ns decreases with temperature, again reflecting a competition between trapping and detrapping during the HP trapping state. These temperature-independent and fast recovery characteristics support the notion that the fast time constant processes that are observed in Figs. 5, 6, and 8 have a common origin. Additional HP-to-ON transients at different  $V_{DG}$  values but the same power dissipation [10] reveal that the fast transients emerge from electrons that were trapped through a hot-electron process. Hot-electron phenomena have also been prominently observed in several other studies [12], [14], [15] along with severe impact on  $R_{ON}$  degradation.

#### IV. IMPACT OF EPITAXIAL GROWTH ON DYNAMIC $R_{ON}$

We have studied the importance of epitaxial growth details on dynamic  $R_{ON}$  characteristics by applying our methodology to identical devices fabricated on a nominally identical epitaxial wafer that was grown by a different commercial

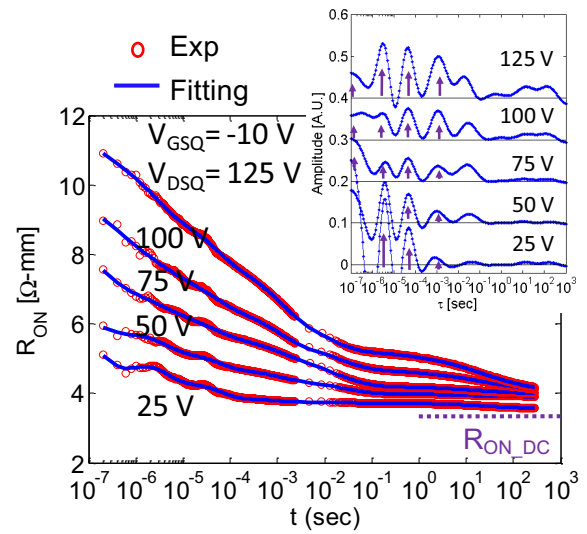


Fig. 9. Dynamic  $R_{ON}$  transients in the alternative wafer (see text) after identical OFF-to-ON switching events, as in Fig. 5, at ambient temperature of 25 °C. Inset: corresponding time-constant spectra. In contrast to Fig. 5, devices in this wafer have much weaker time constants in longer time periods, whereas short time constants in the submicrosecond to millisecond range dominate and do not change as  $V_{OFF}$  increases.

epitaxial vendor. The device layer stack comprising GaN cap, AlGaN barrier, AlN spacer, and GaN channel layer follows an identical design with the same AlGaN mole fraction and thicknesses. Most likely, there are differences in buffer structure design which is the proprietary information of each epitaxy-growth supplier and is unknown to us. This alternative wafer was processed into devices in the same lot with the same layout as the sample discussed earlier in this paper. The breakdown voltage of these new devices is  $> 200$  V.

A different buffer could well result in a different defect structure in the top active layers that produce different dynamic  $R_{ON}$  characteristics as evaluated by our methodology. As is the case for the wafer discussed earlier, many different devices have been tested and the results are consistent. The observed differences shown here between devices from the two wafers reflect wafer-to-wafer differences.

Dynamic  $R_{ON}$  transients under identical OFF-to-ON switching conditions as in Fig. 5 have been measured in a device from this alternative wafer at ambient temperature of 25 °C and are shown in Fig. 9. The observed pattern of  $R_{ON}$  recovery is rather different from those shown earlier. In contrast to the dominance of long time constants in the data of Fig. 5, the alternative wafer exhibits much weaker time constants for longer time periods whereas short time constants in the submicrosecond to millisecond range dominate. This is clearly seen in the time constant spectra shown in the inset of Fig. 9. These measurements show that these two wafers have a rather different defect structure.

Dynamic  $R_{ON}$  measurements at different ambient temperatures following trapping at  $V_{GSQ} = -5$  V and  $V_{DSQ} = 40$  V in the alternative wafer are shown in Fig. 10. These data are equivalent to those of Fig. 6 earlier in this paper. Once again we find that the recovery transients with short time constants

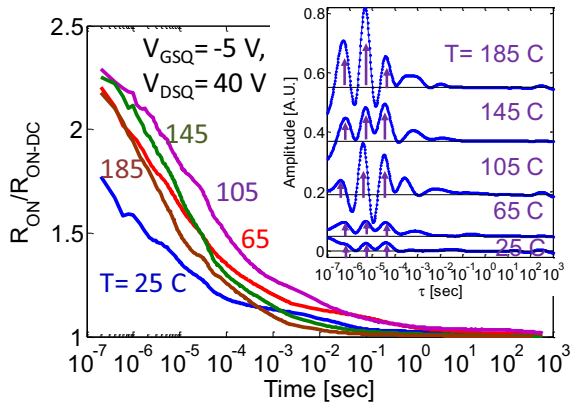


Fig. 10. Top:  $R_{ON}/R_{ON,DC}$  transients in devices from the alternative wafer at different ambient temperatures for  $V_{GSQ} = -5$  V and  $V_{DSQ} = 40$  V. The resulting time constant spectra (inset) show that the dominant transients with short time constants are temperature-independent.

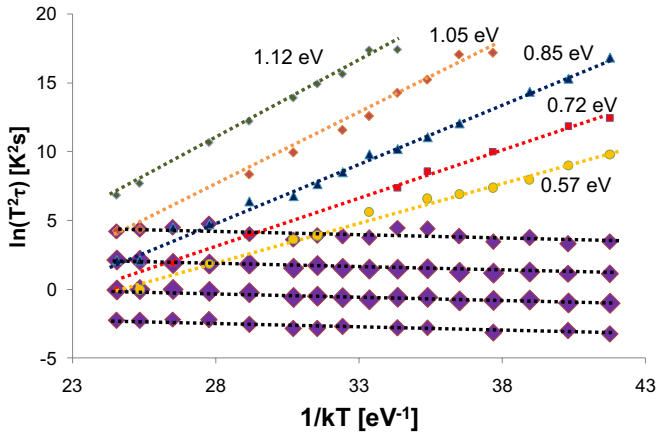


Fig. 11. Arrhenius plot of time constant spectra of Fig. 10. The size of the symbols is proportional to the height of the time constant peak. A rich spectrum of traps with activation energies between 0.57 and 1.12 eV is observed, but their concentration is much lower than that in Fig. 7. The dominant time constants are short and do not exhibit any temperature dependence.

change little with temperature. This temperature-independent behavior is also verified in the corresponding spectra in the inset of Fig. 10.

An Arrhenius plot for the dominant time constants of Fig. 10 is shown in Fig. 11. As shown in Fig. 7, the size of the symbols indicates the magnitude of corresponding time constant. In this alternative wafer, a richer spectrum of traps with energies between 0.57 and 1.12 eV is observed but their concentration is much lower than in Fig. 7. The short time constants are clearly dominant in this wafer and they are again temperature-independent.

These results reveal that there are at least two distinct mechanisms that dominate dynamic  $R_{ON}$  transients at short times and at long times. The long time transients are associated with conventional traps. The noticeable differences in the two wafers indicate that these can be engineered through proper growth protocols. The short time transients arise from a different mechanism and both the wafers suffer from it. This suggests that they might be associated with an intrinsic aspect of heterostructure.

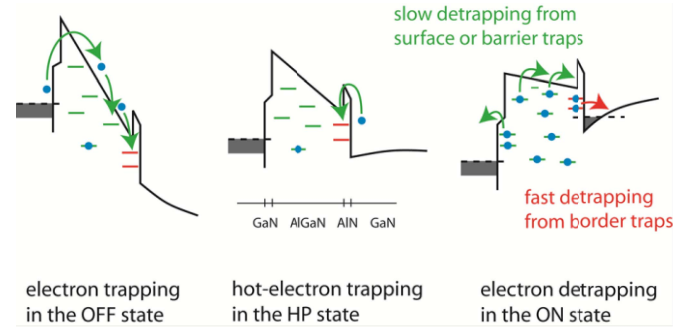


Fig. 12. Postulated mechanisms responsible for dynamic  $R_{ON}$  of GaN HEMTs observed in this paper. In the OFF state, electron-trapping at the surface, in AlGaN and at AlGaN/AlN interface, takes place as the electrons flow outside the gate. In the HP state, hot electrons from the channel are trapped at AlGaN/AlN interface states. In the ON state, electron-detrapping takes place thermally for traps in the AlGaN or at the surface and through a tunneling process for AlGaN/AlN interface traps (border traps).

## V. MECHANISMS RESPONSIBLE FOR DYNAMIC $R_{ON}$

Our methodology when applied to GaN HEMTs on SiC reveals a rich dynamic behavior of  $R_{ON}$ . A picture that can explain all the experimental observations described earlier is shown in Fig. 12. In the OFF state, electrons are trapped as they flow outside the gate into the AlGaN barrier and eventually into the channel (Fig. 12, left). These electrons can be trapped inside AlGaN, at the surface or at the interface states at the AlGaN/AlN interface right above the channel [16]. In the HP state, on the other hand, electrons in the channel gain kinetic energy and overcome the energy barrier with the AlGaN and get trapped. possible sites for this trapping process are interface states at the AlGaN/AlN interface right above the channel (Fig. 12, middle).

During the detrapping process that follows OFF state biasing, we observe fast temperature-independent detrapping processes as well as long thermally activated detrapping processes. On the other hand, after HP-state trapping, only fast temperature-independent detrapping is observed. This suggests that the fast processes observed in both the cases have the same origin and that detrapping takes place through a tunneling process. This is consistent with detrapping from interface states at the AlGaN/AlN spacer interface [16], [17]. Traps that are physically located behind a barrier, but very close to the channel and that release their electrons through a tunneling process, are known as border traps [18]. We postulate that AlGaN/AlN interface states behave as border traps as the AlN layer is very thin. The longer thermally activated time transients observed after OFF-state trapping are associated with conventional traps at the surface on the gate-drain gap or inside the AlGaN barrier. These are accessible from the gate in the OFF state but not from the channel in the high-power state because of the relatively large electric field across the AlGaN barrier.

The defects at the AlGaN/AlN interface are perhaps intrinsic to the nature of this interface and the high stress under which AlN is grown. If our hypothesis is correct, this detrapping mechanism could be eliminated through the removal of AlN spacer layer.

Many studies have been devoted to buffer trapping which depends on the various types of traps that are introduced during the growth process [19]. Some buffer trapping could be present in the devices that are studied. Separation of buffer trapping, barrier trapping, and surface trapping is an important topic that is explored by other techniques [20]. The dynamic  $R_{ON}$  characterization methodology proposed in this paper should also be helpful to study this issue.

## VI. CONCLUSION

In summary, we have developed a new methodology to investigate  $R_{ON}$  transients over arbitrary lengths of time. We have used this new technique to study trapping effects in high-voltage GaN HEMTs under a variety of pulsing conditions. In OFF-to-ON time transients, dynamic  $R_{ON}$  is enhanced up to several times of the original dc value, particularly as the OFF-state voltage increases. We have identified two distinct mechanisms with different timescales and temperature behavior. On a short timescale, the fast release of trapped charge takes place through a temperature-independent tunneling process. We postulate that interface states at the AlGaIn barrier/AlN spacer interface are responsible for this. Conventional thermally assisted detrapping follows on a longer timescale. This postulate occurs from traps at the surface or inside the AlGaIn barrier. In contrast, after a high power to ON switching, only fast detrapping through a temperature-independent process is observed. This is also consistent with trapping at the AlGaIn/AlN interface. These findings provide a path to engineer a reliable GaN power-switching transistor with minimum dynamic  $R_{ON}$  problems.

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