

# **Models for Pattern Dependencies: Capturing Effects in Oxide, STI, and Copper CMP**

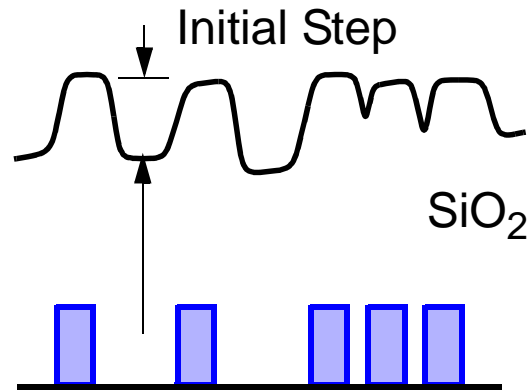
**Duane Boning, Brian Lee,  
Tamba Tugbawa, and Tae Park  
MIT Microsystems Technology Laboratories**

**Semicon West  
July 17, 2001**

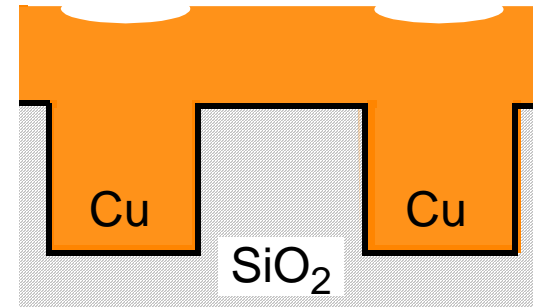
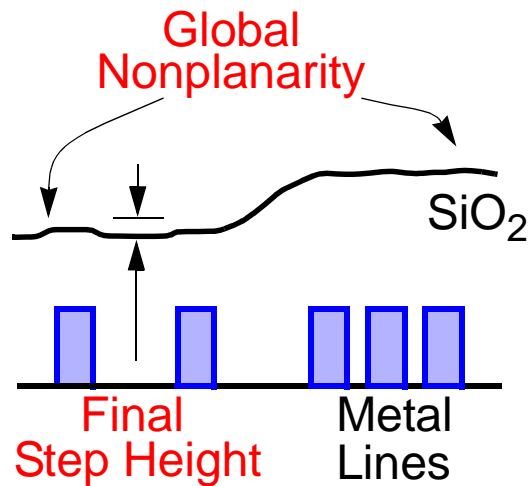
# Outline

- Motivation: Pattern Dependencies in Oxide, STI, and Metal Polishing
- Pattern Effects and Models
  1. Pattern density: planarization length and density averaging
  2. Deposition profile: lateral bias of layout for conformal/HDP deposition
  3. Step height: local feature contact height and rate vs. height dependence
  4. Nanotopography: contact wear model for film thinning
  5. Dual material selectivity: extensions to density/step-height model
  6. Initial plating topography: integrated contact wear & density/step-height
  7. Multilevel copper polish: integrated contact wear & density/step-height
  8. Alternative consumables - fixed abrasives: non  $K/\rho$  density dependence
- Current and Future Challenges

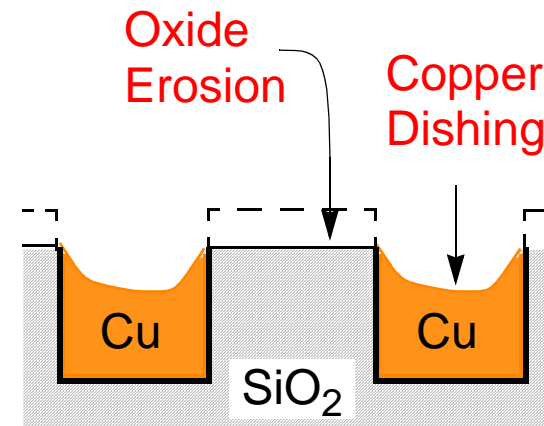
# Pattern-Dependent CMP Concerns



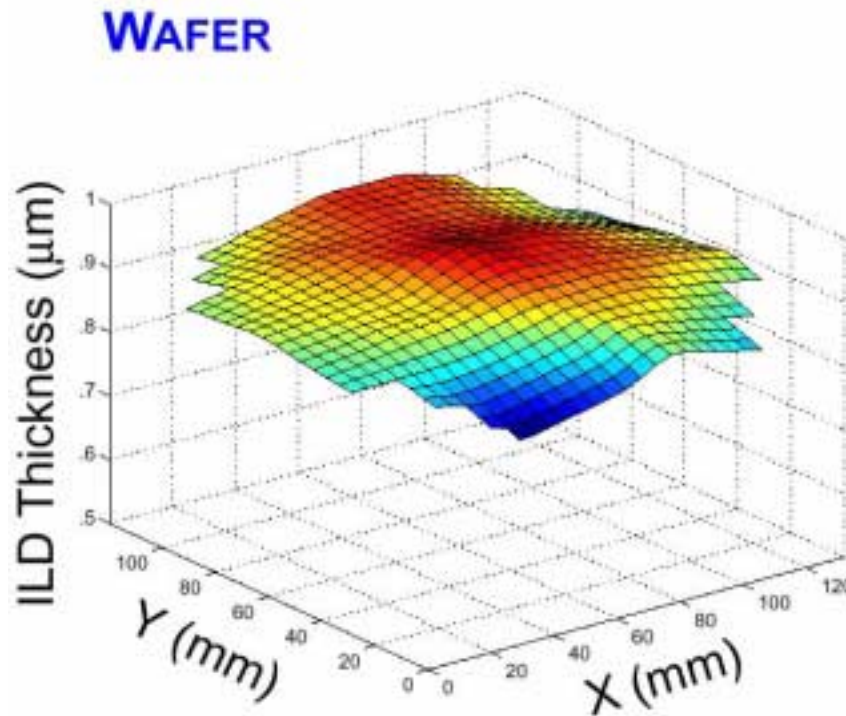
Oxide  
CMP:



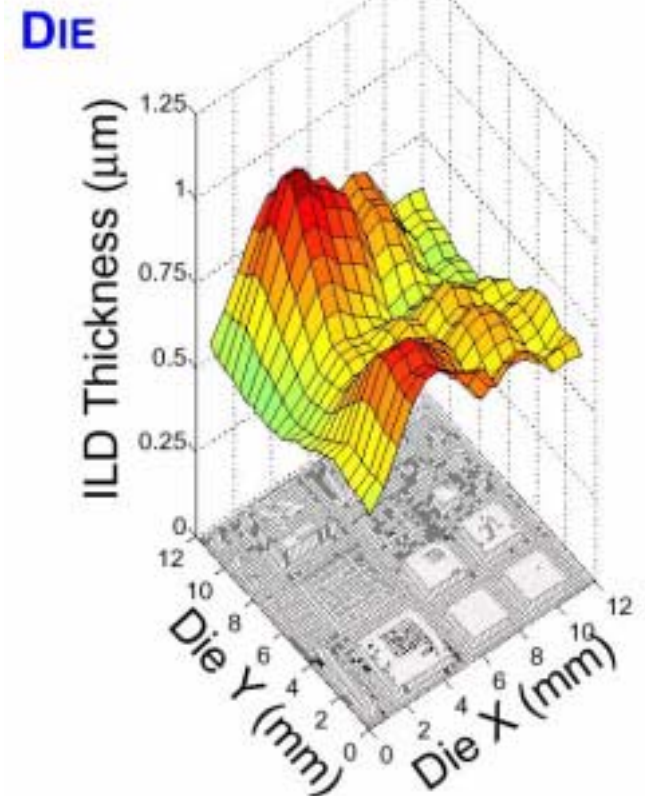
Copper  
CMP:



# Wafer-Level vs. Die-Level CMP Modeling



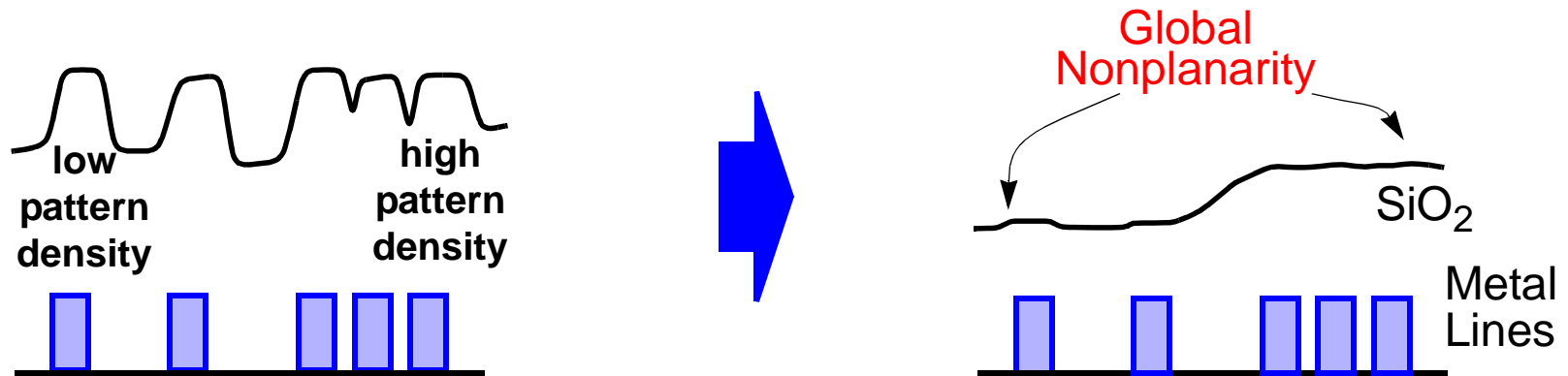
- **Across wafer uniformity**  
depends on process parameters, tool design, consumable wear
- Mechanics & fluids models



- **Within die uniformity**  
depends on layout pattern, pad/slurry, process parameters
- **Chip and feature-scale models**

# 1. Pattern Density Effects

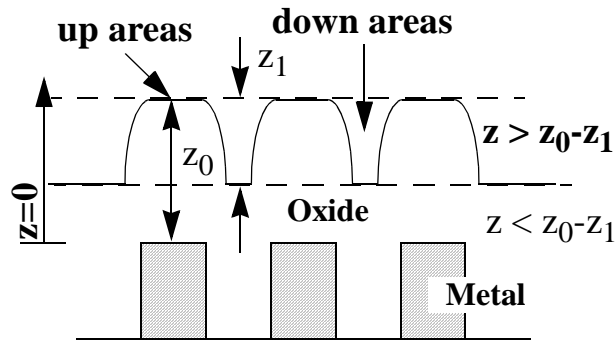
- Basic Idea: up area removal depends on area fraction (pattern density):



1. **Polish rate** at each location on the die is **inversely proportional** to the effective pattern density
2. **Effective pattern density** at each point depends on the nearby topography and layout density
3. The effective pattern density can be determined by averaging over a **planarization length** (or planarization window)
4. The planarization length must be **characterized** or **extracted** for a given CMP consumable set and process

Stine et al., CMPMIC '97

# Oxide CMP Pattern Dependent Model (Stine et al. '97)



- Removal rate inversely proportional to density

$$\frac{dz}{dt} = -k_p \rho v = -\frac{K}{\rho(x, y)}$$

- Density assumed constant (equal to pattern) until local step has been removed:

$$\rho(x, y, z) = \begin{cases} \rho_0(x, y) & z > z_0 - z_1 \\ 1 & z < z_0 - z_1 \end{cases}$$

- Final oxide thickness related to effective density:

$$z = \begin{cases} z_0 - \left( \frac{Kt}{\rho_0(x, y)} \right) & Kt < \rho_0 z_1 \\ z_0 - z_1 - Kt + \rho_0(x, y) z_1 & Kt > \rho_0 z_1 \end{cases}$$

- $z$  = final oxide thickness over metal features
- $K$  = blanket oxide removal rate for a die of interest
- $t$  = polish time
- $\rho_0$  = local pattern density

- Evaluation of pattern density  $\rho_0(x, y)$  is key to model development

# Effective Density Calculation and Planarization Length Extraction

MIT Integrated Dielectric Characterization Mask

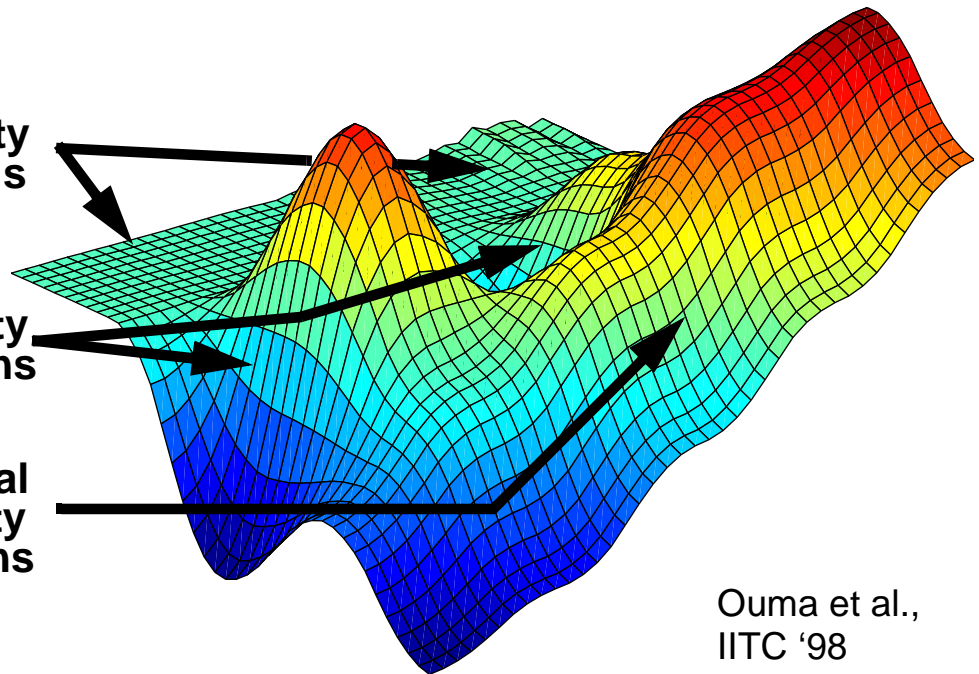


Post-CMP Oxide Thickness (Up Areas)

50% density regions

step density regions

gradual density regions



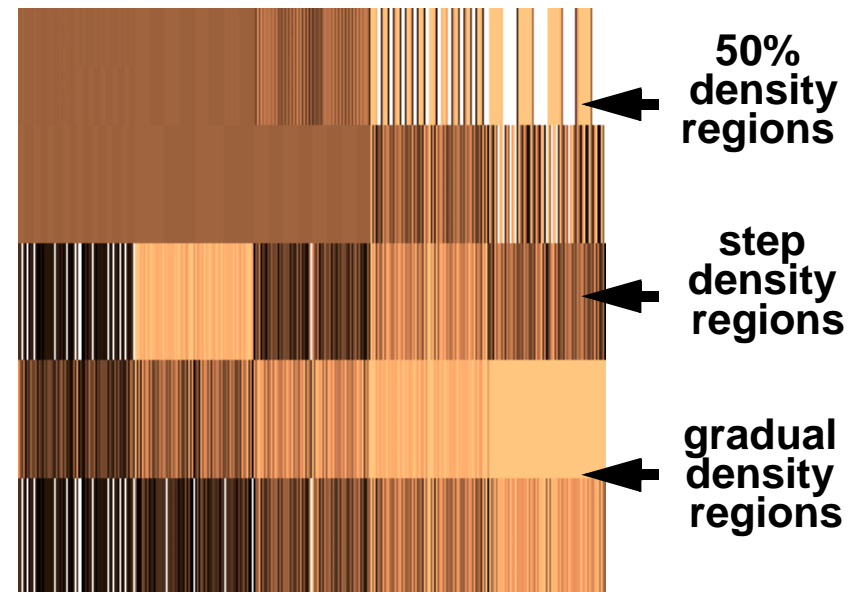
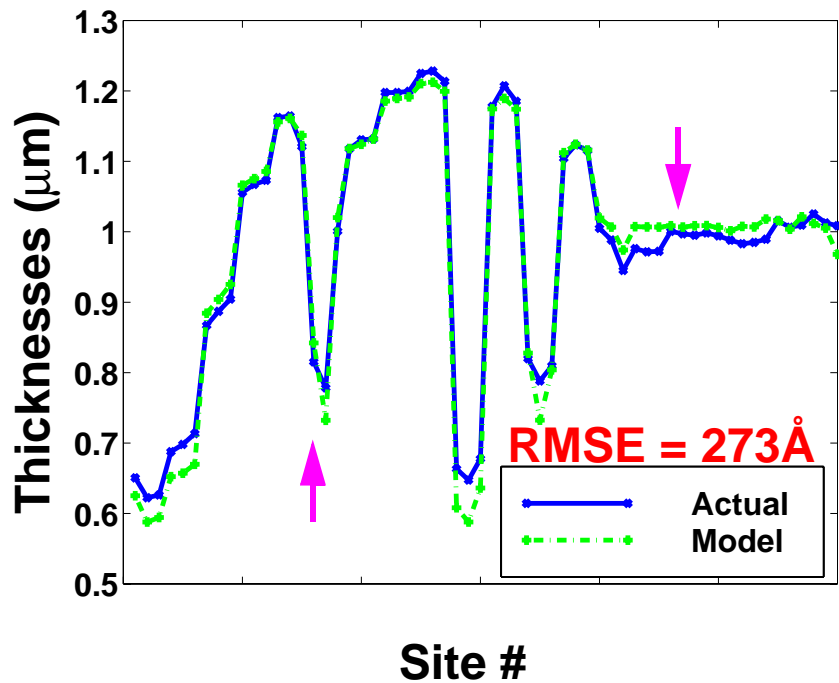
Ouma et al.,  
IITC '98

- Use circular weighted window (based on deformation of an elastic material) to calculate average or effective density  $\rho$  for each point on die
- Effective density determines polish rate: 
$$RR = \frac{K}{\rho(x, y, PL)}$$

# Example: Post-Oxide Polish Thickness Prediction

- Density dependent model applied to “up” (over metal) oxide thickness resulting from oxide CMP:

## Raised Area Predictions



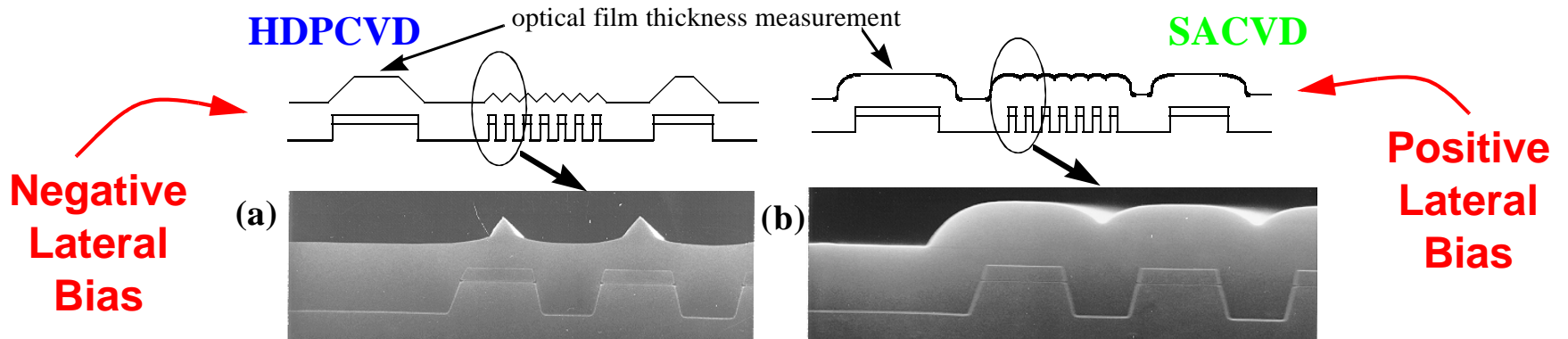
gradual density regions      step density regions      50% density regions

Smith et al.,  
CMP-MIC '99

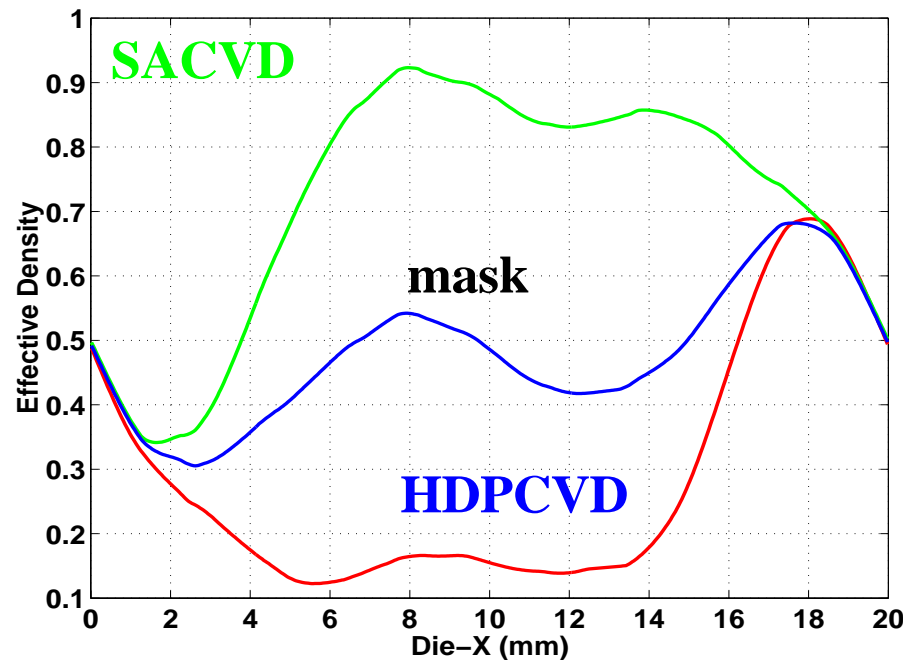
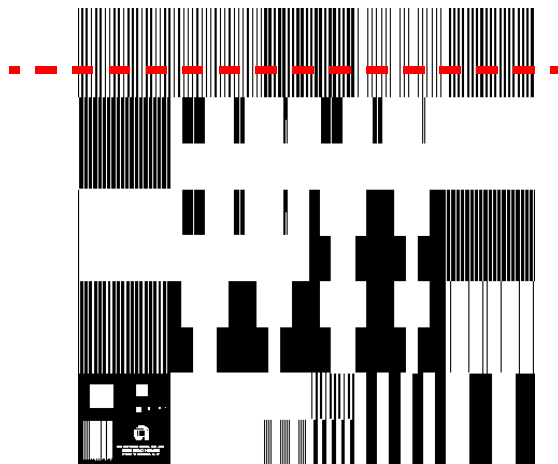


# 2. Deposition Profile Effects

- Oxide topography is critical (especially for STI CMP)



- Effective density model for oxide polish



T. Pan et al., VMIC '98

# 3. Step Height Dependent Effects

- **Incompressible Pad Model:**

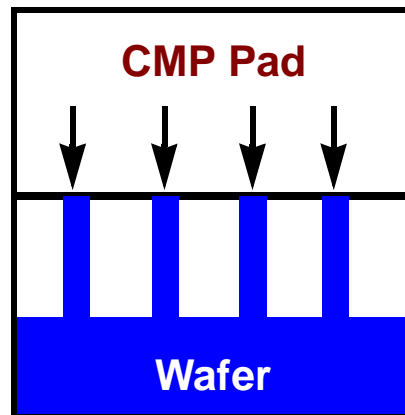
- Up area removal rate scaled by density (e.g. MIT density model)

- **Compressible Pad Model:**

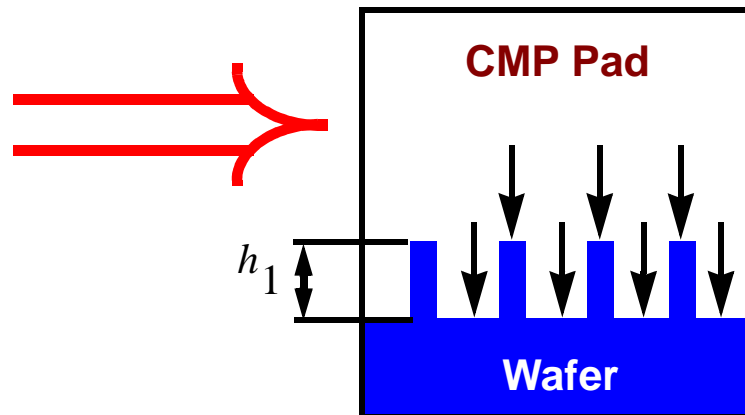
- Up area removal rate proportional to step height (Burke, Tseng, others)

- **Transition** from incompressible to compressible pad model (Grillaert et al. - IMEC)

- Occurs at contact height  $h_c$  or contact time  $t_c$  where  $h_c = h_0 - \left( t_c \cdot \frac{K}{\rho} \right)$



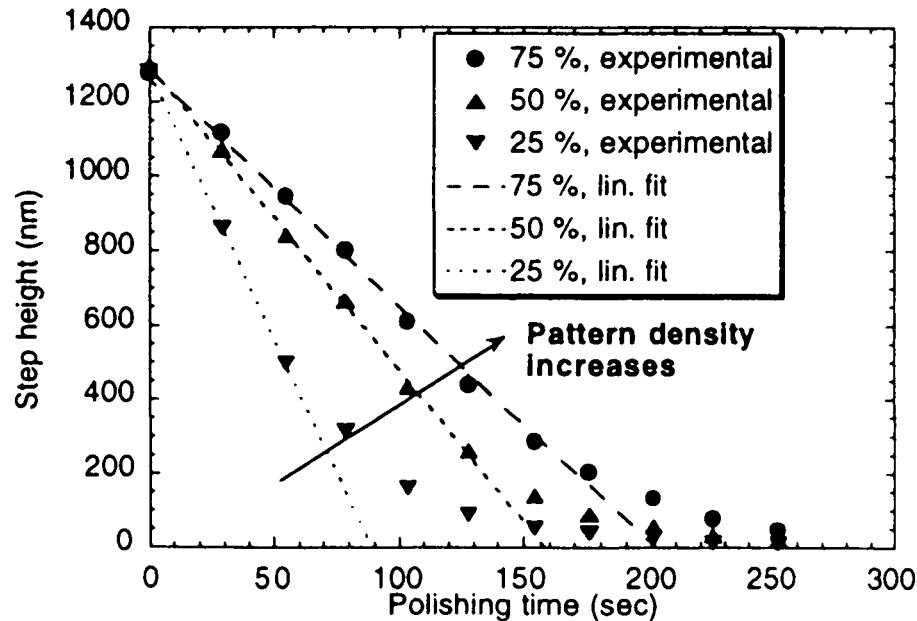
**Incompressible Pad Model**



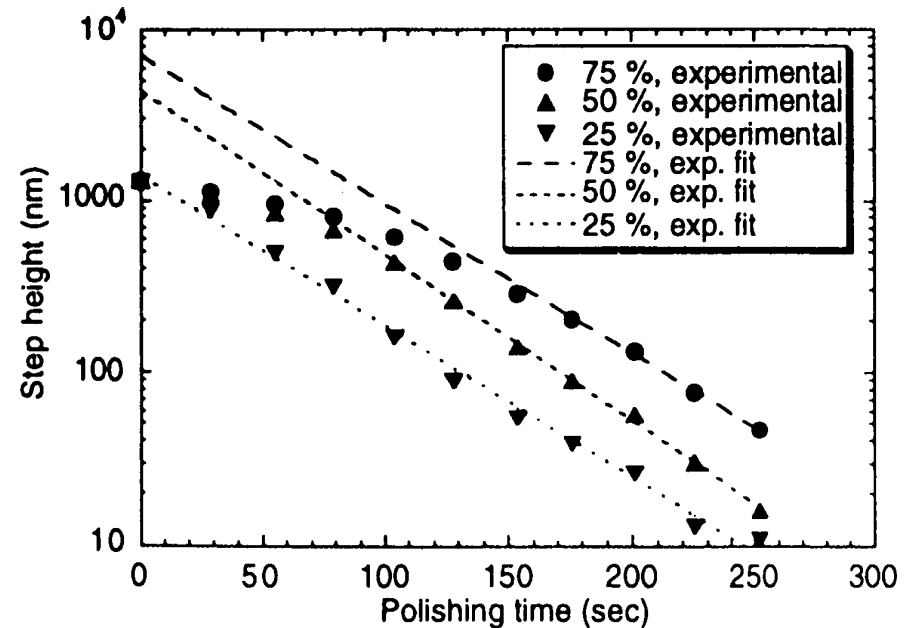
**Compressible Pad Model**

# Step Height Reduction

## Large Step Heights



## Small Step Heights



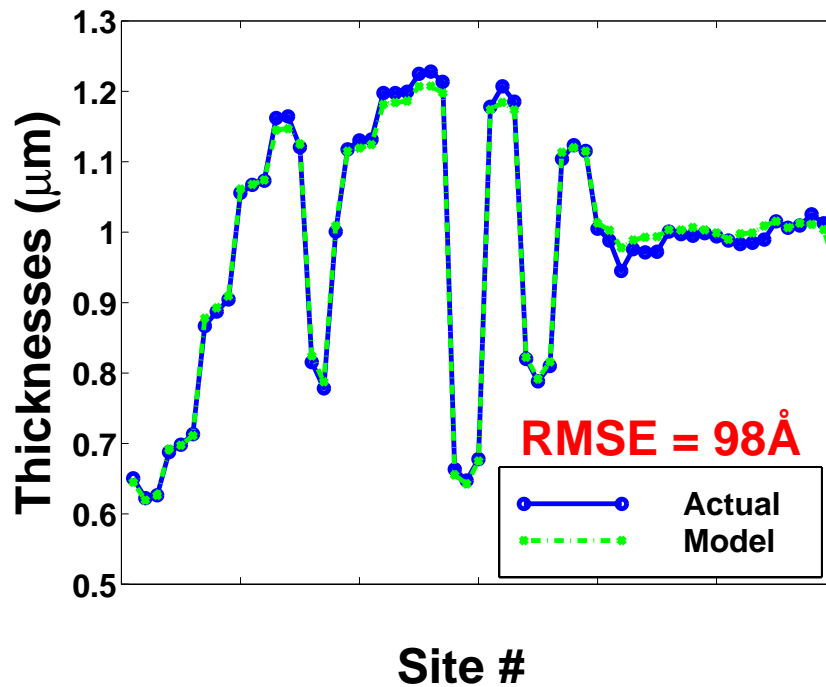
- Density effect dominates
- Step height reduction **linear** in time

- Up/down area pressure difference
- Step height reduction **exponential** in time

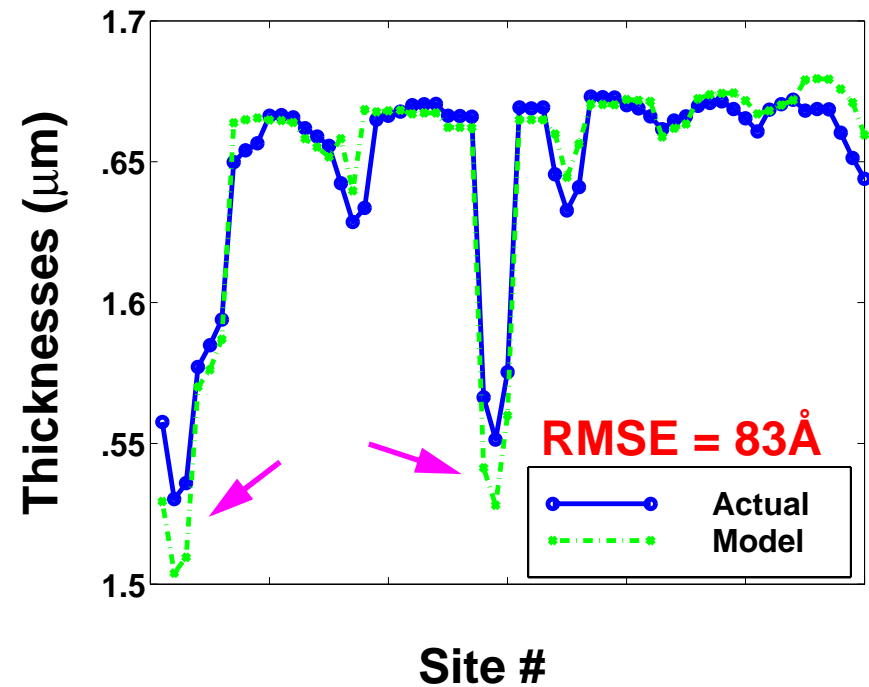
Grillaert et al., CMP-MIC '98

# Results: Integrated Density/ Step Height Model

## Raised Area Predictions



## Down Area Predictions



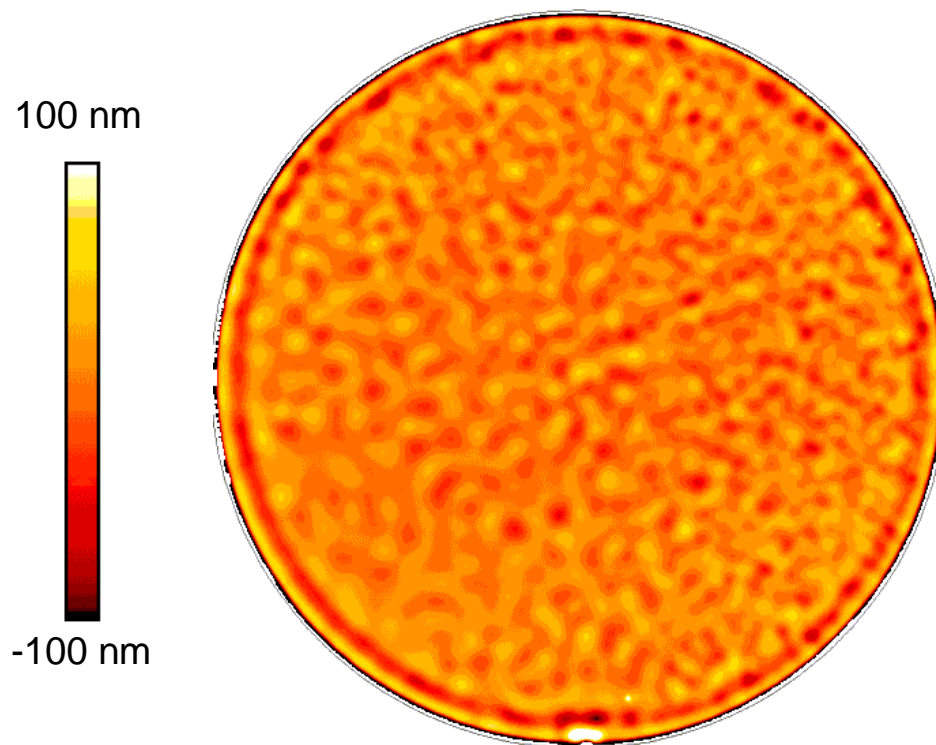
Smith et al.,  
CMP-MIC '99

- Dramatically reduced errors:
  - 273 Å rms (density model) --> 98 Å RMSE (integrated model)
- Challenge:
  - Over-predicts down polish at low density: macro bending limit?

## 4. Wafer Nanotopography Effects

“Nanotopography” refers to wafer surface variations with:

1. Lateral length scales from 0.2 mm to 20 mm
2. Height variations ~ 10 to 100 nm

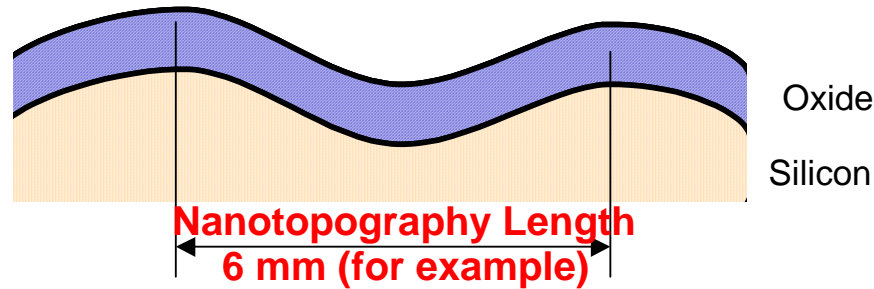


### Nanotopography Map: 8” SSP Silicon Epi Wafer

Filtered data measured using  
a NanoMapper™ production  
nanotopography tool at ADE  
Phase Shift in Tucson, AZ

# Nanotopography vs. Planarization Length

Given nanotopography variations on some length scale...



What happens during CMP?

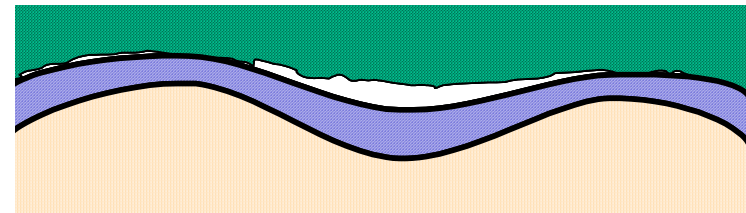
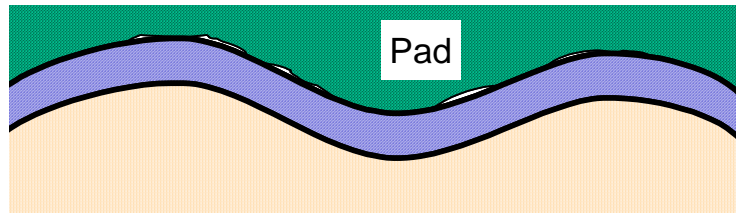


CMP



"Soft" Pad CMP Process  
Planarization Length ~ 3-4mm

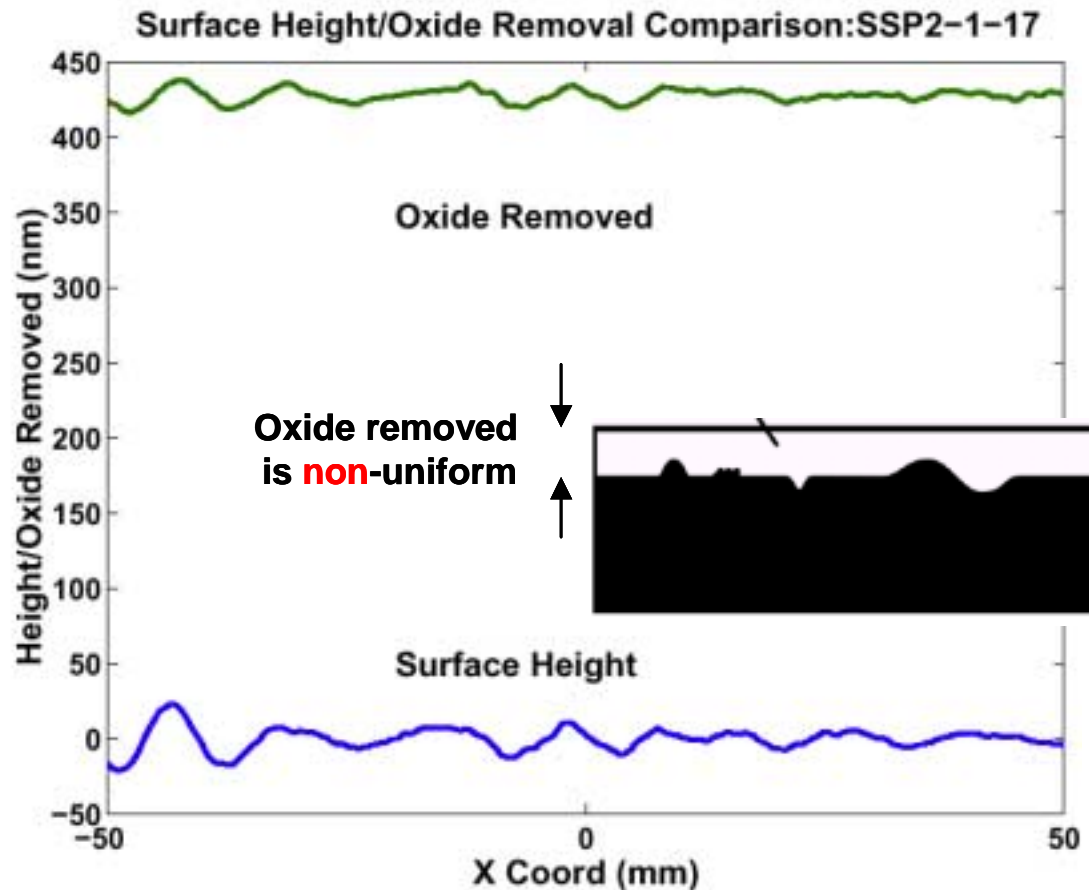
"Stiff" ("Hard") Pad CMP Process  
Planarization Length ~ 7-10 mm



- pad conforms around nanotopography variations and polishes uniformly

- pad "bridges" across nanotopography down areas and preferentially thins surface films in raised nanotopography areas

# Example: Short NL and Long PL (Stiff Pad)



## Split Details

- IC1000 solo pad (8.5mm planarization length)
- SSP2 wafer (short-range nanotopography)

## Result

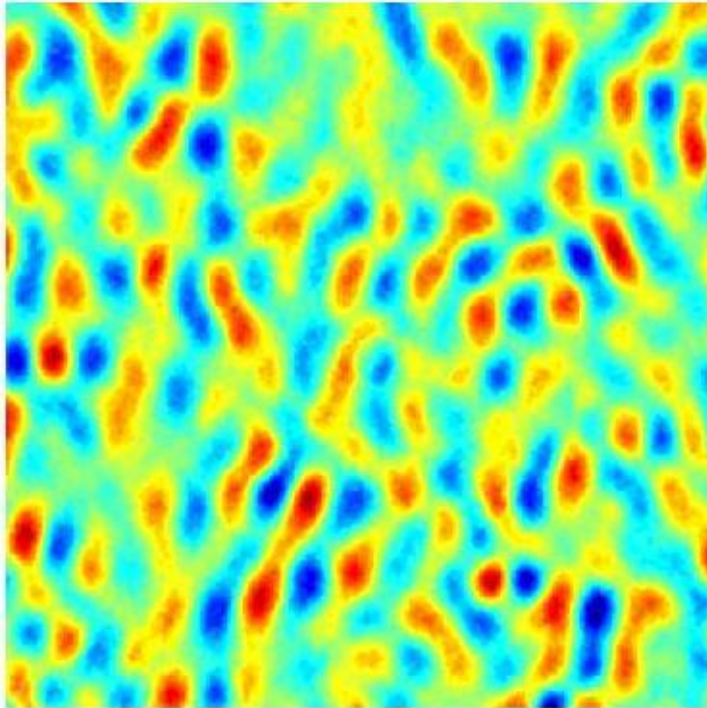
- Nanotopography *propagates* strongly into oxide film
- Filtered data used (removes wafer scale polish non-uniformity)



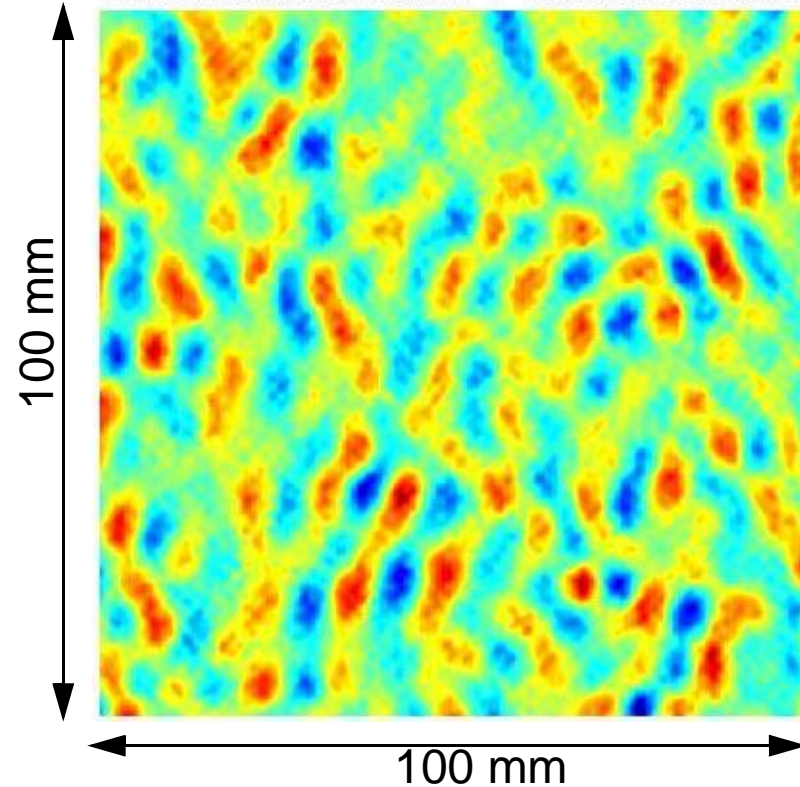
# Short NL and Long PL (Stiff Pad) - cont'd

- SSP2 wafer; IC1000 solo pad, process has PL = 8.5 mm
- Variation for central 100mm portion of wafer
  - Deviation in each normalized: full range variation around each mean shown

Central Region for:SSP2-1-17, height variation



Central Region for:SSP2-1-17, oxide removed





# Nanotopography Modeling

## ■ Density/Step-Height Model Difficulties:

### □ Pattern Density

- generally refers to area fraction of equal height patterned features
- no clear definition in case of nanotopography

### □ Step Height

- in density/step-height model, the step height is a local parameter (i.e. applying to micron-scale features)
- in nanotopography, structures with gentle (long range) step height variations

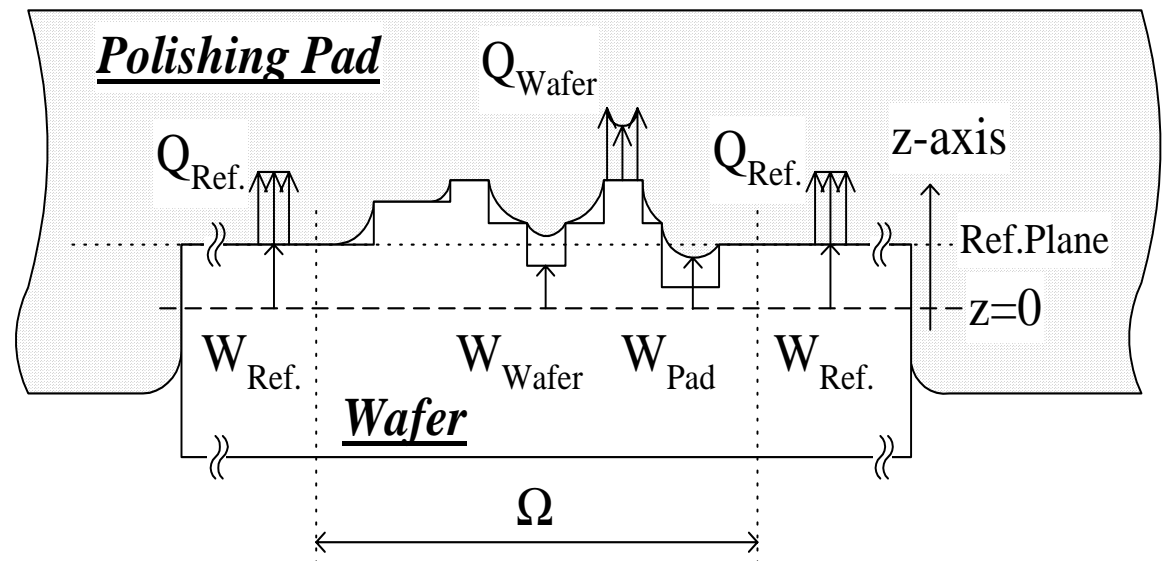
## ■ Alternative Modeling Approach: Contact Wear

### □ Goal: account for the specific configuration of nanotopography features on CMP:

- compute effect of height differences on long-range pad pressure distributions
- explicitly account for pad bending and pressure apportionment

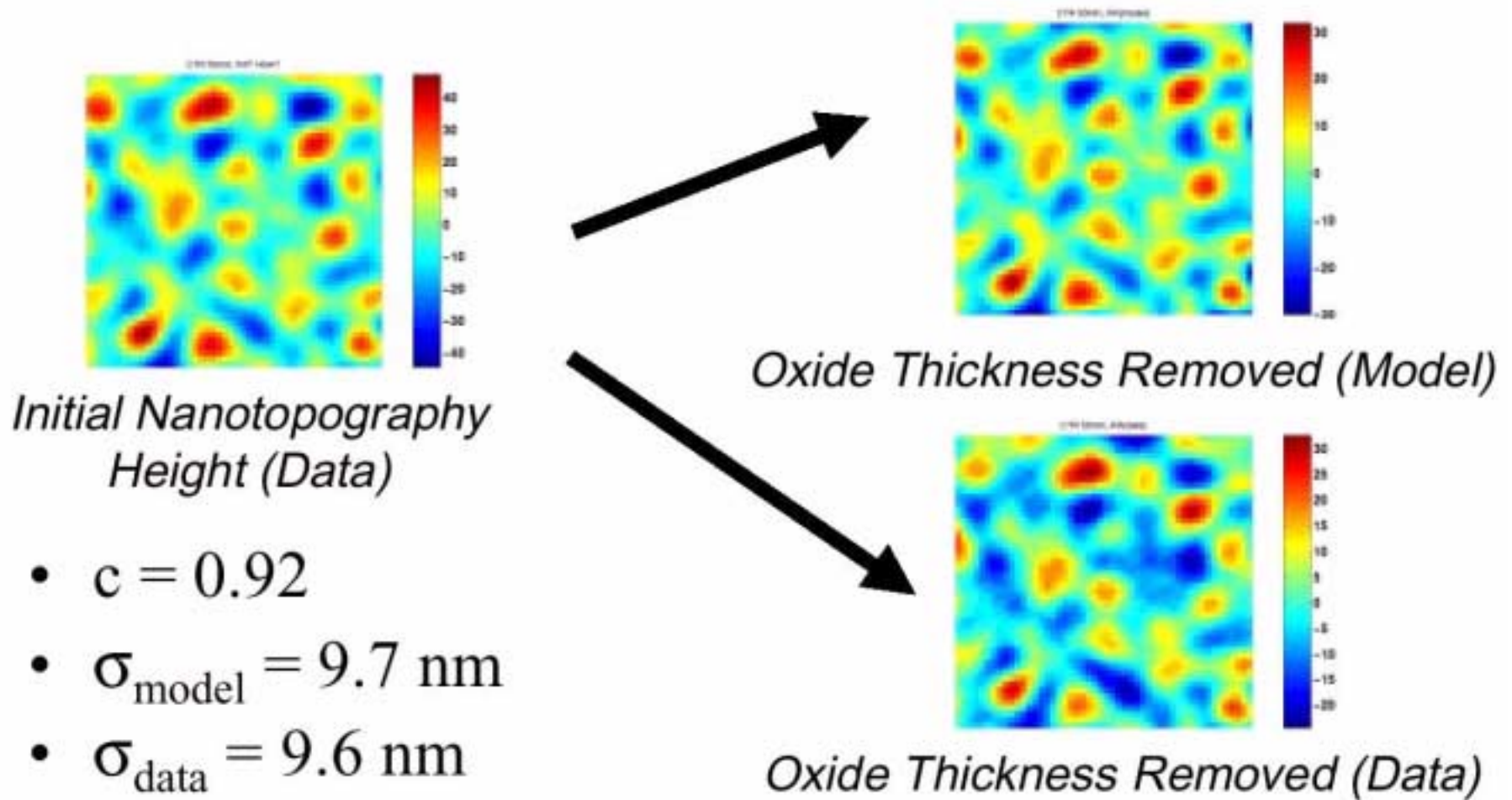
# Contact Wear Model

- Treat the polishing pad as an elastic body: displacement function of load
- Discretized boundary elements are considered with boundary conditions:
  - $w$  - localized heights/displacements
    - when pad contact wafer,  $q$  unknown,  $w_{i, known} = W_{Ref} - W_{i, wafer}$
  - $q$  - localized pressures
    - when pad not in contact,  $w$  unknown,  $q_{i, known} = Q_{Ref}$
- Solve for pressures and displacements at each point in time, gives removal rate and advancement of the boundary element



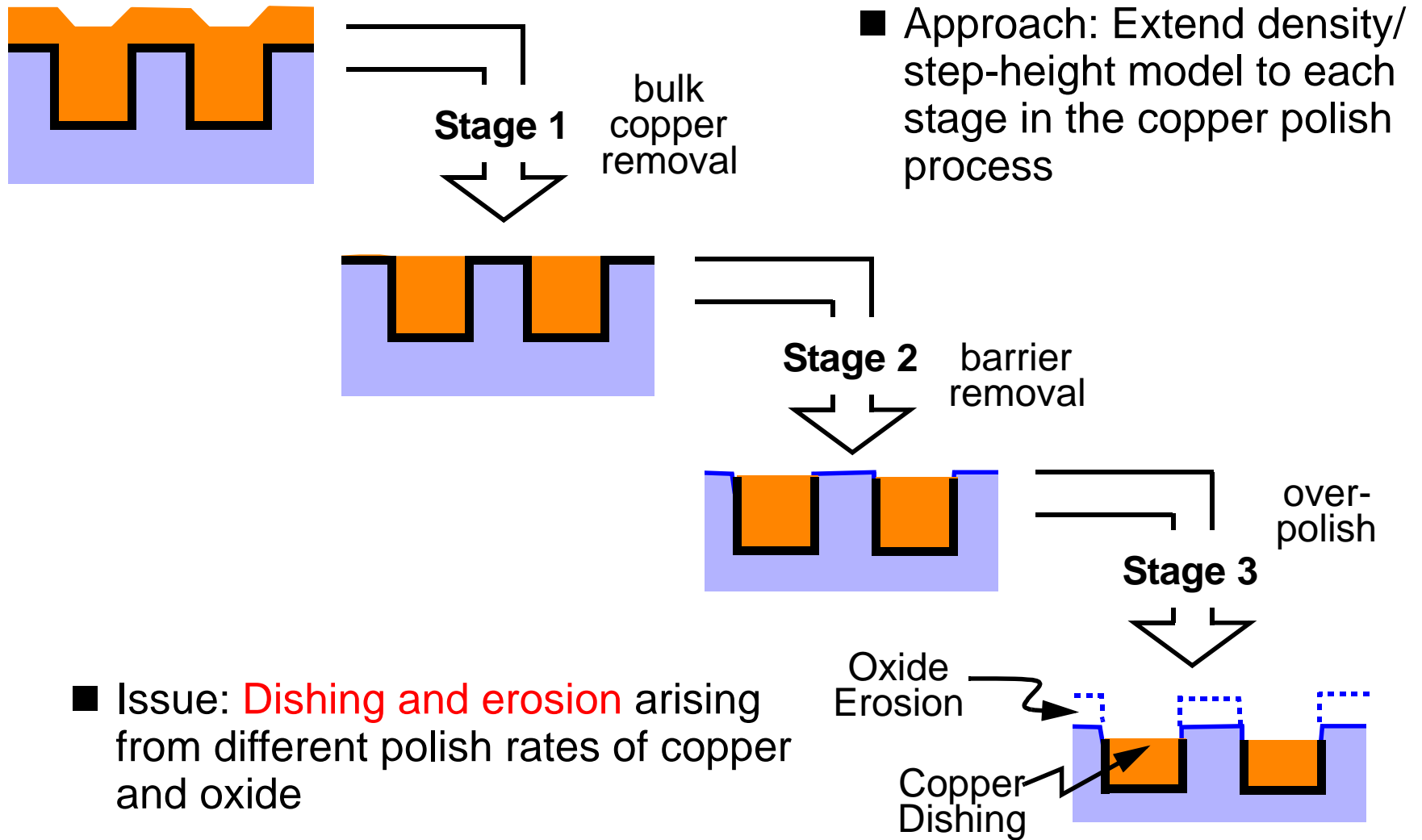
T. Yoshida, *ECS PV 99-37*, 1999.

# Results: Contact Wear Nanotopography/CMP Model



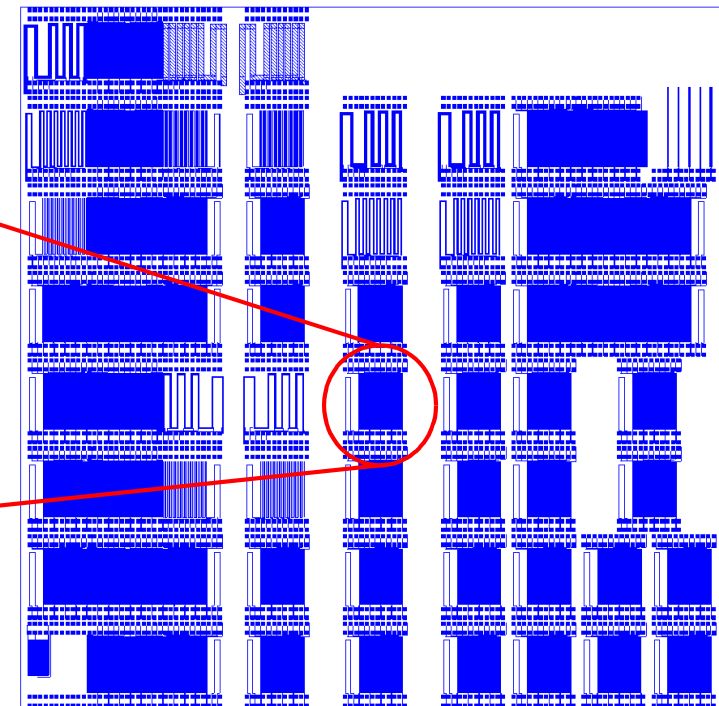
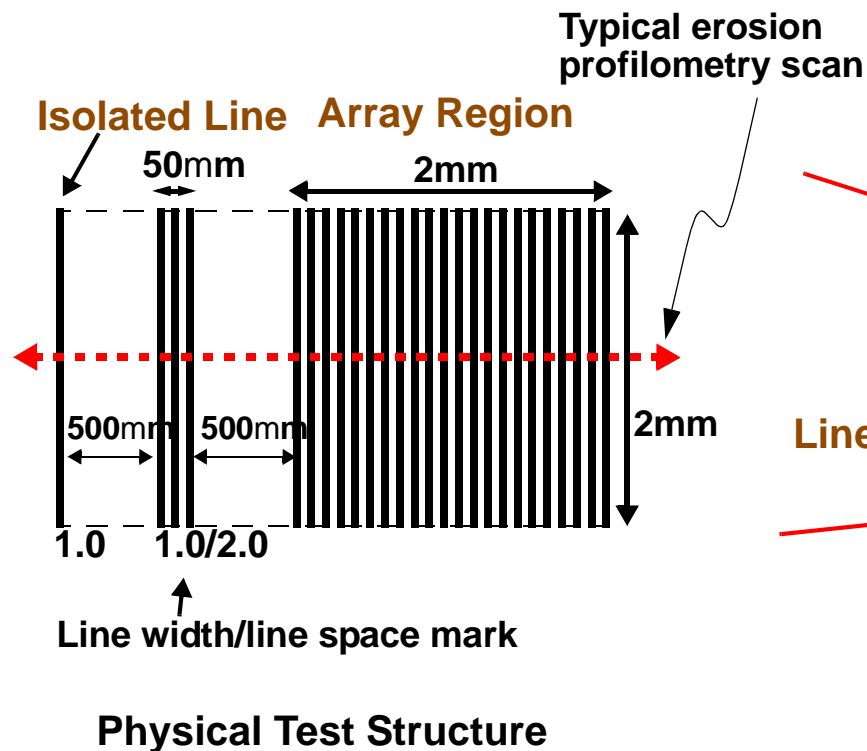
Lee et al., MRS 2001.

# 5. Copper CMP: Dual Material Polish Effects



# Test Structures and Test Masks: Dishing and Erosion Characterization

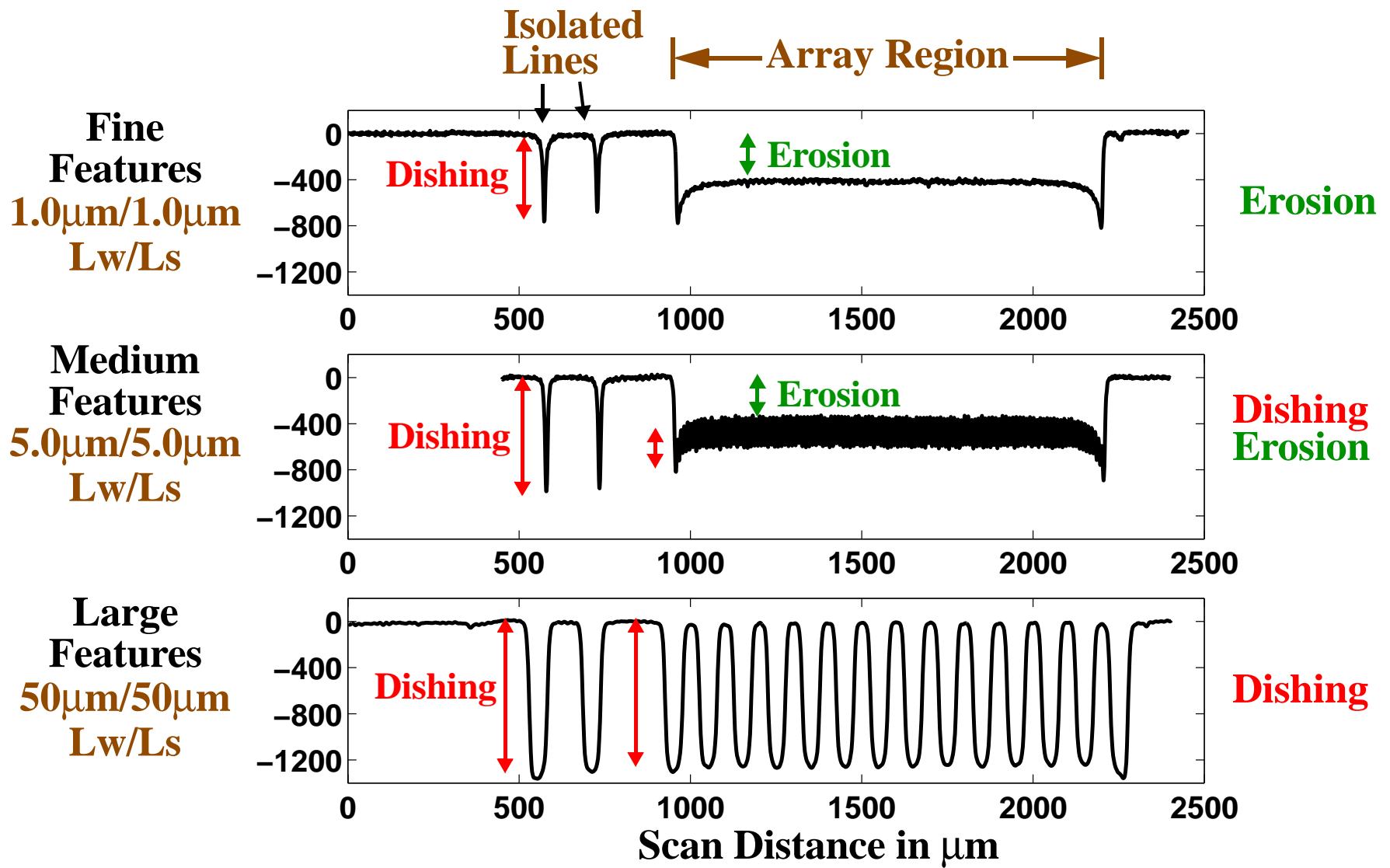
## Metal 1



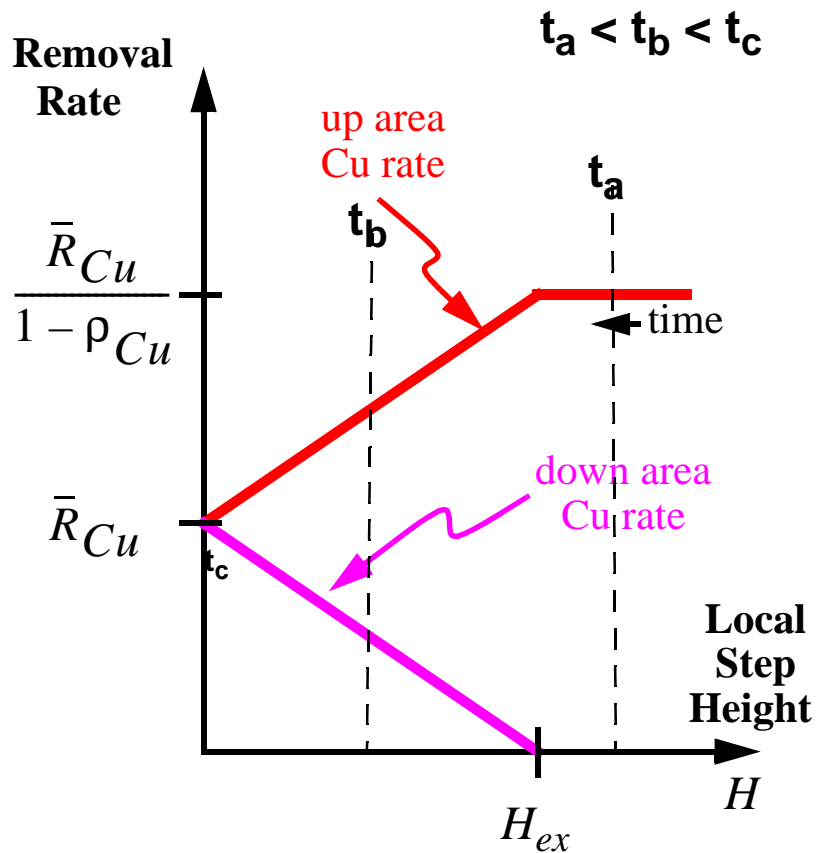
- Single level effects: Layout factors on M1 to study creation of topography
  - density
  - line width & line space combinations

# Copper Dishing and Erosion Trends

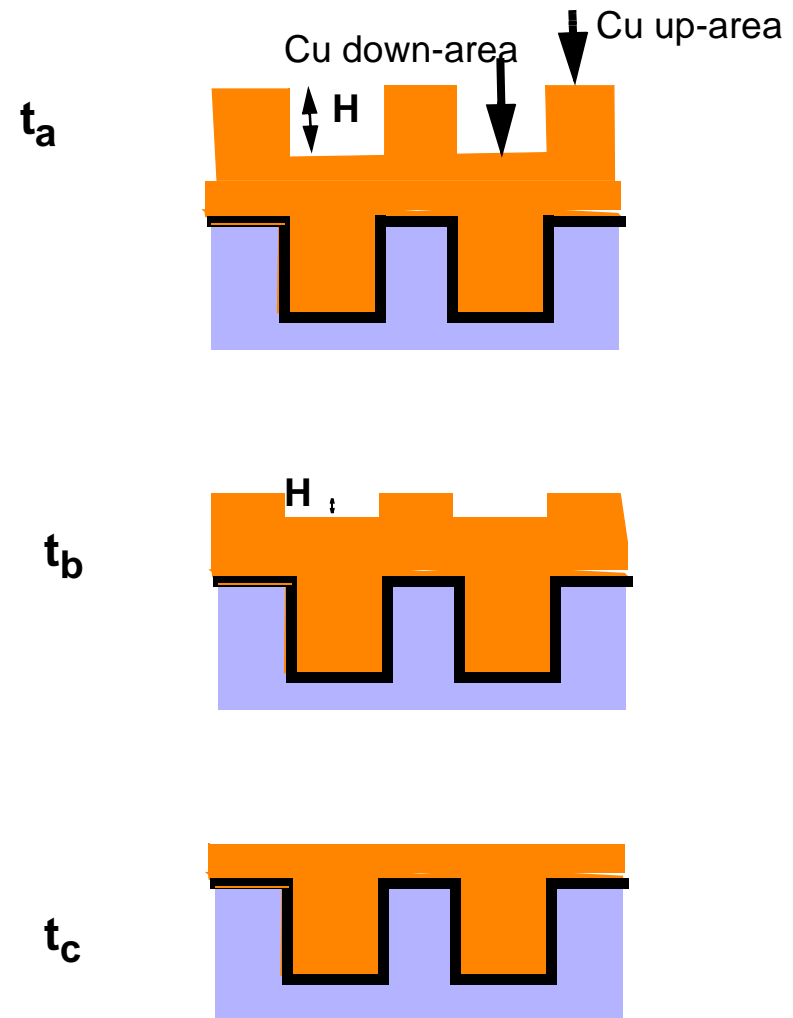
## Surface Profiles (in Å)



# Cu CMP Modeling -- Stage 1: Removal of Overburden Cu

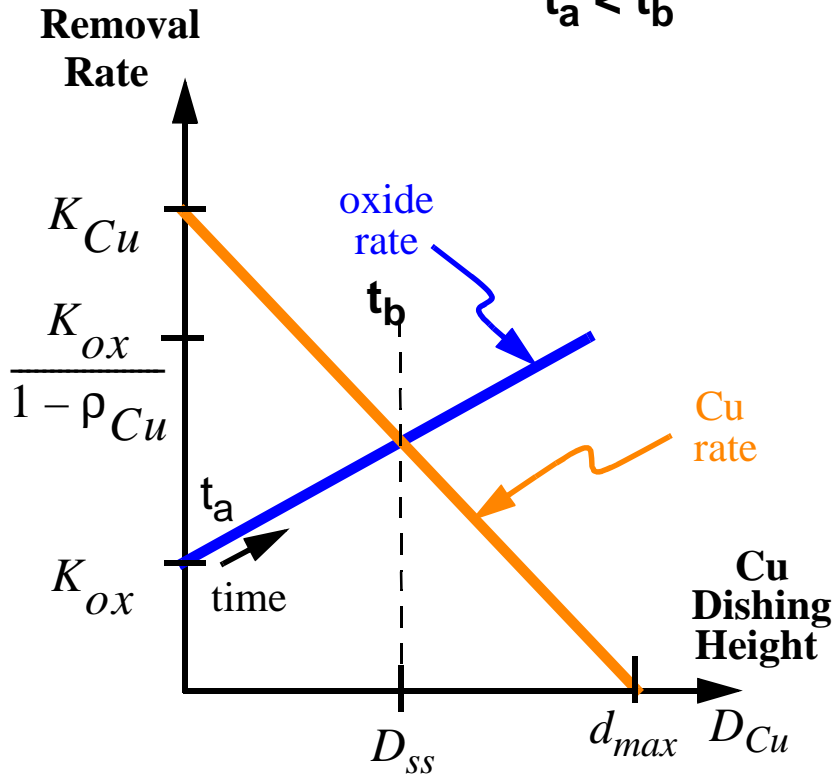


- $H_{ex}$ : Local step height above which the pad does not contact the down area.

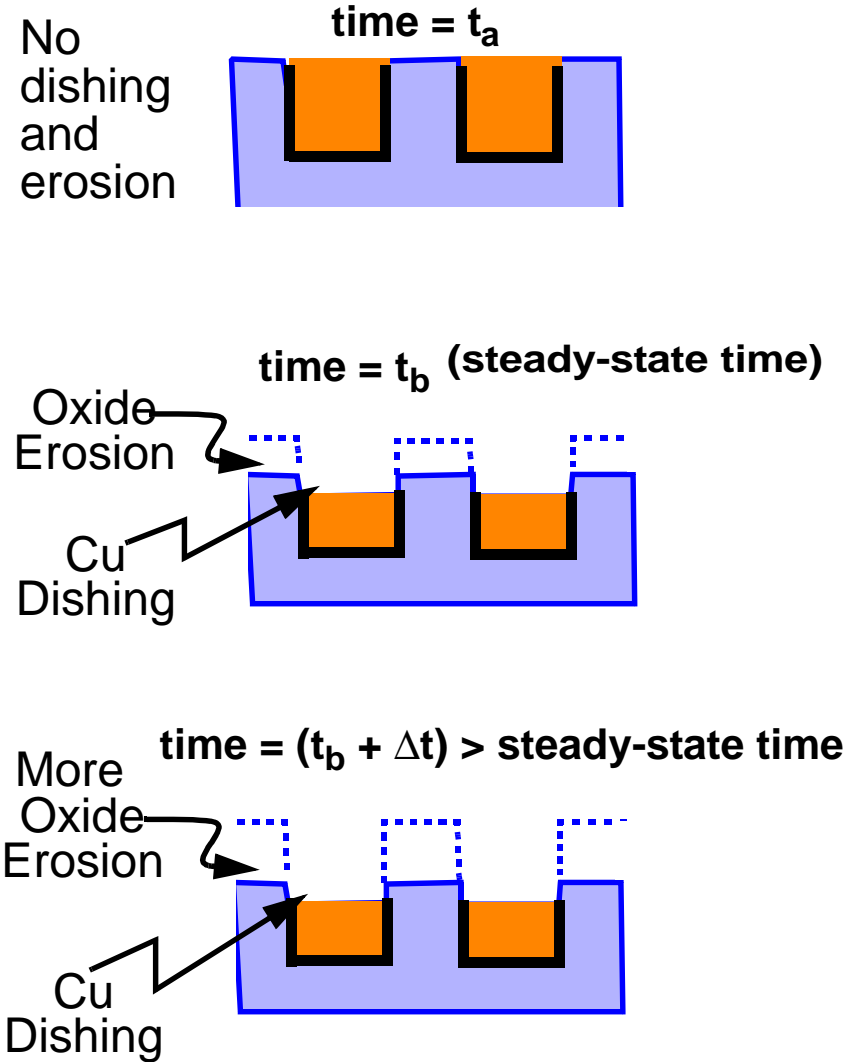


# Cu CMP Modeling -- Stage 3: Overpolish

$$t_a < t_b$$



- $D_{ss}$  is steady-state Cu dishing.
- $D_{Cu}$  is Cu dishing.
- $d_{max}$  is maximum Cu dishing.

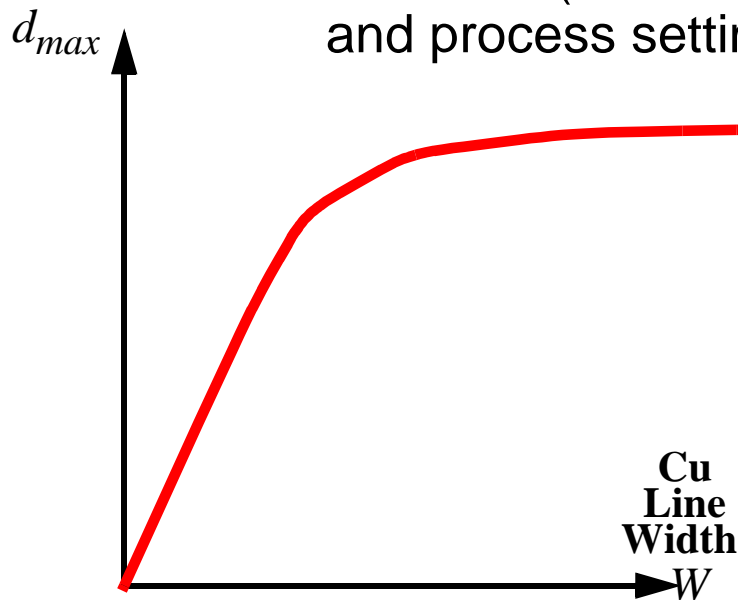




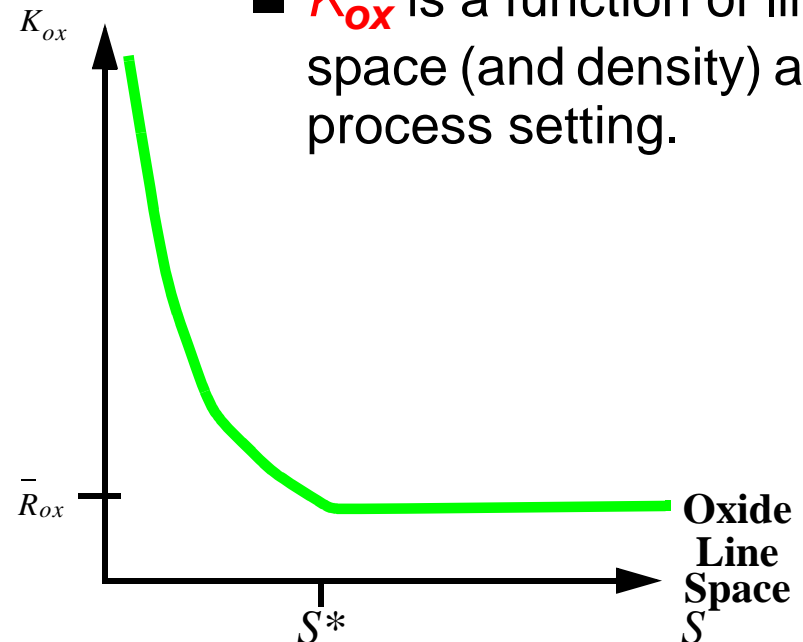
# Cu CMP Model Parameters

- The model parameters (unknowns) are  $K_{ox}$ ,  $K_{Cu}$ ,  $K_b$ ,  $d_{max}$ , and  $H_{ex}$ . These parameters depend on Cu line width or oxide line space, pattern density and process parameters (down force, table speed, slurry, pad elasticity, etc.).
- For a given process, these model parameters can be estimated from time evolution experiments done with specially designed test masks.

- $d_{max}$  is a function of line width (and density) and process setting.

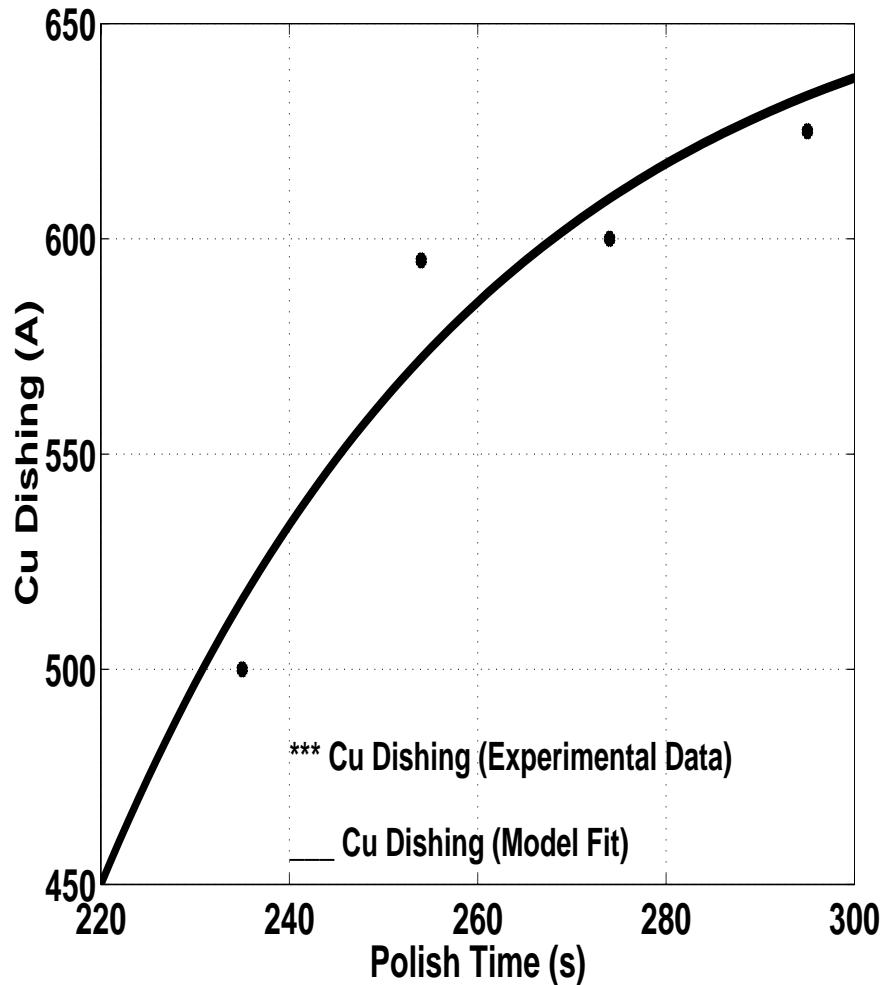


- $K_{ox}$  is a function of line space (and density) and process setting.

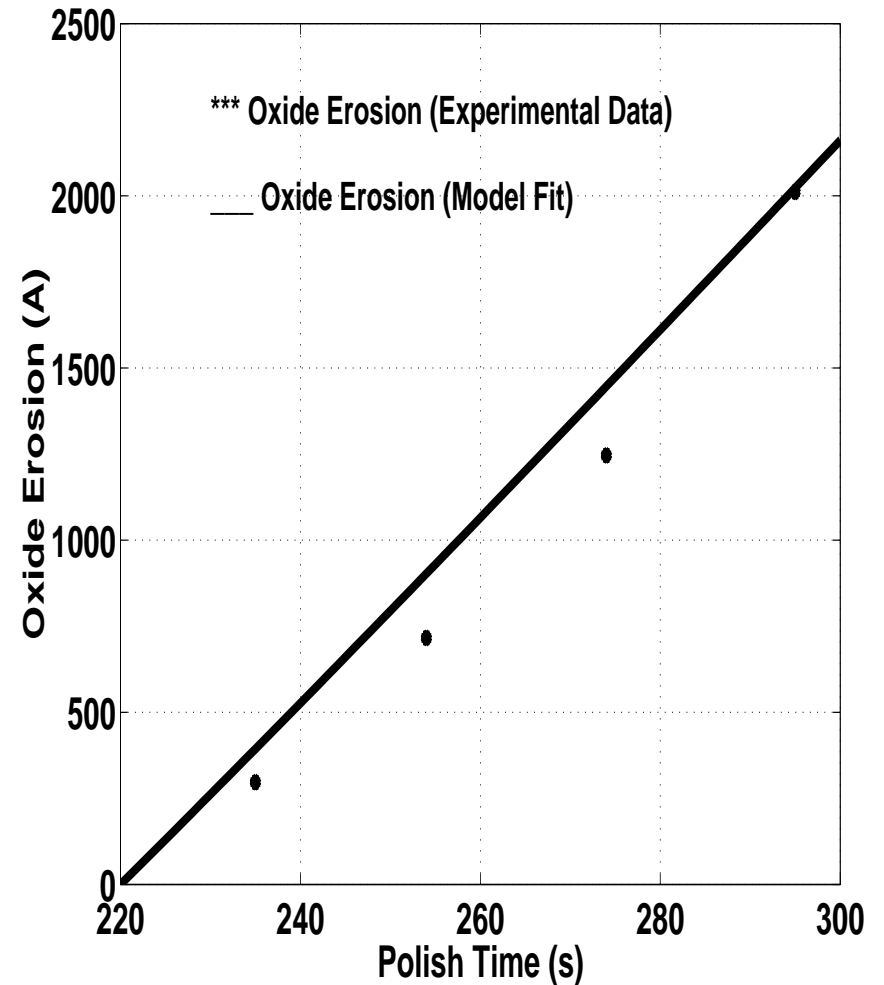


# Experimental Data versus Model: Cu Dishing/Erosion Time Trend

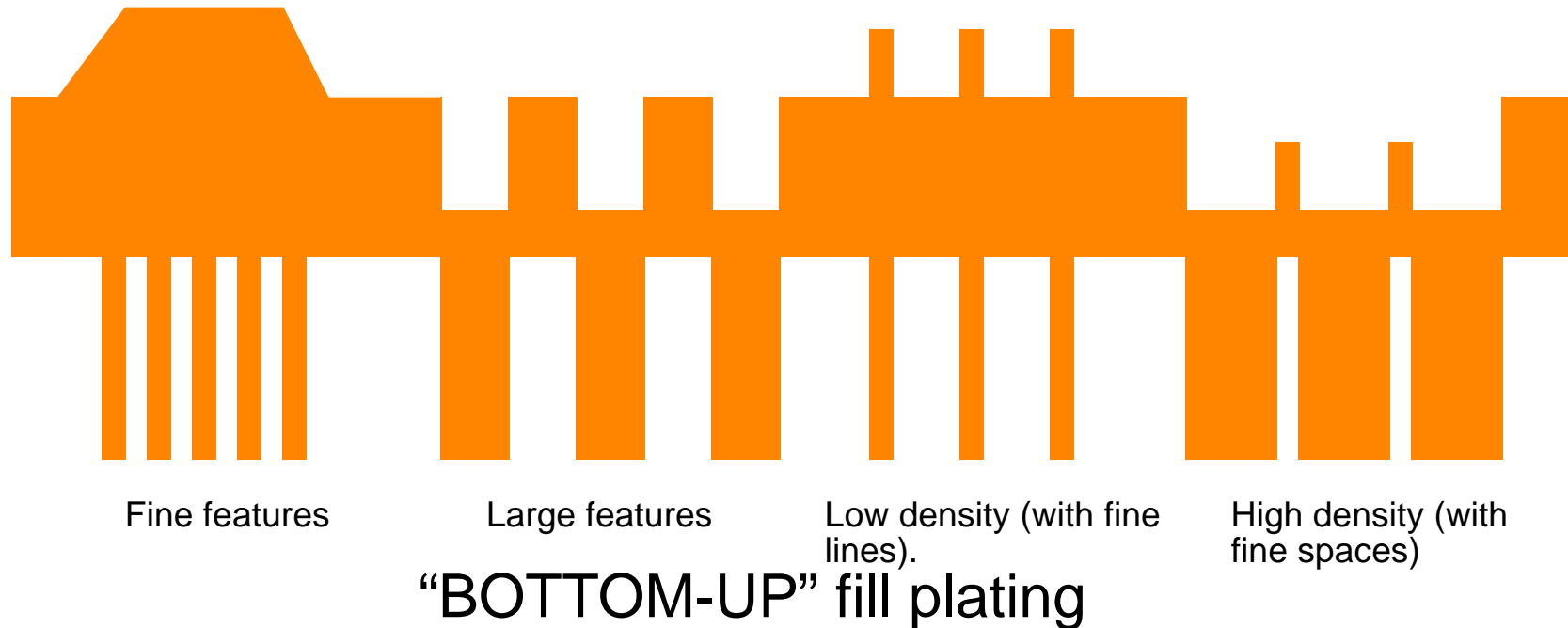
Dishing versus polish time for line width of 10  $\mu\text{m}$  and density of 50%.



Erosion versus polish time for line space of 10  $\mu\text{m}$  and density of 50%.

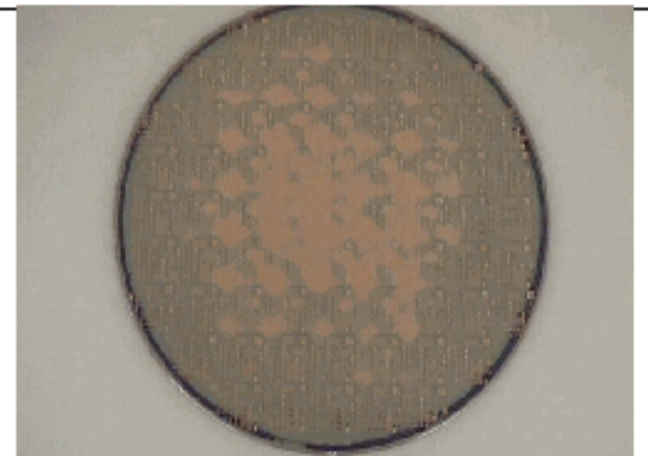


# 6. Copper Electroplating Topography Effects



- Topography leads to excessive overpolish which causes:
  - ❑ Excessive metal loss (dishing plus erosion).
  - ❑ Surface non-uniformity

Tugbawa et al., MRS 2001.



# Contact Wear vs. Density/Step-Height

- Density/Step-Height Model
  - Excellent for local effect prediction
  - Does not take into account global step-heights
- Contact Wear Model
  - Excellent for long-range pressure apportionment
  - Computationally prohibitive if discretization is down to the feature level

INTEGRATED MODEL

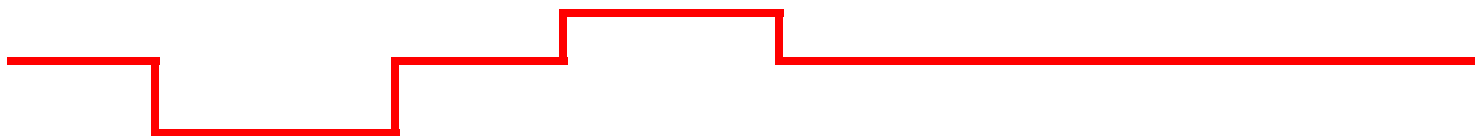
Tugbawa et al., MRS 2001.

# Integrated Contact Mechanics and Density/Step-Height Model

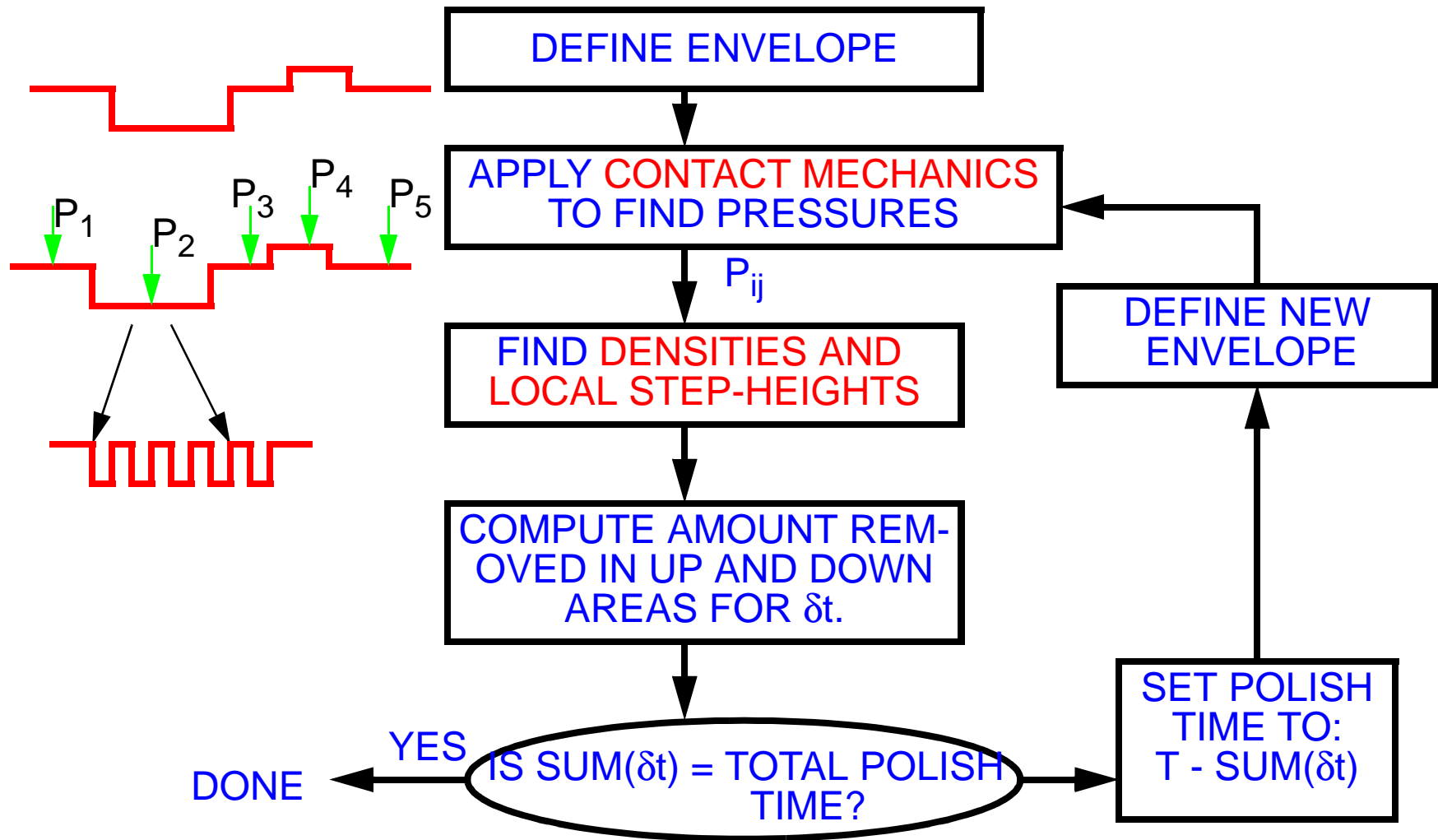
- Consider the following problem in the bulk copper clearing stage:



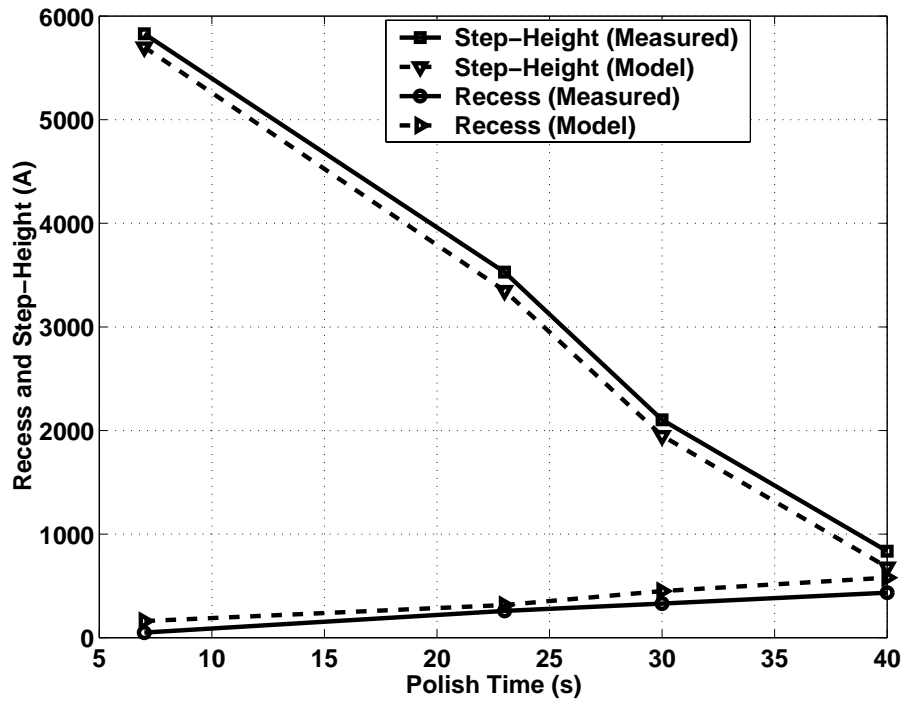
- Define an “envelope” which gives the relative heights of the local “up-areas” across some large scale (coarsely discretized) region
  - Use contact wear model to determine pressures *across* each of these large scale regions
  - Use density/step-height model to determine up/down area removal rate *within* each region



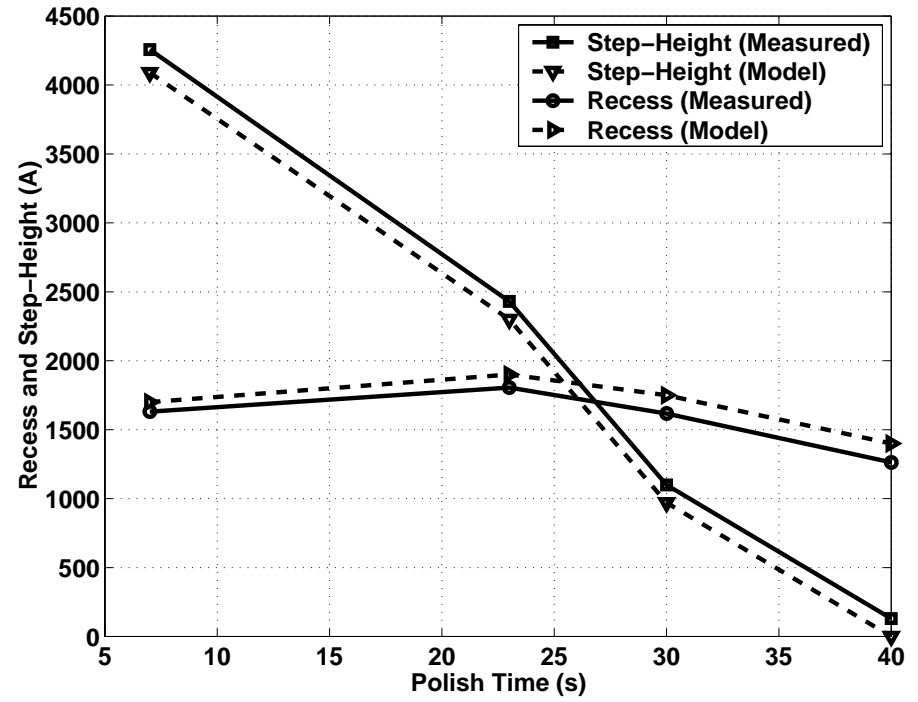
# Integrated Contact Mechanics and Density/Step-Height Model, cont'd



# Results: Stage 1 (Bulk Copper Polish)



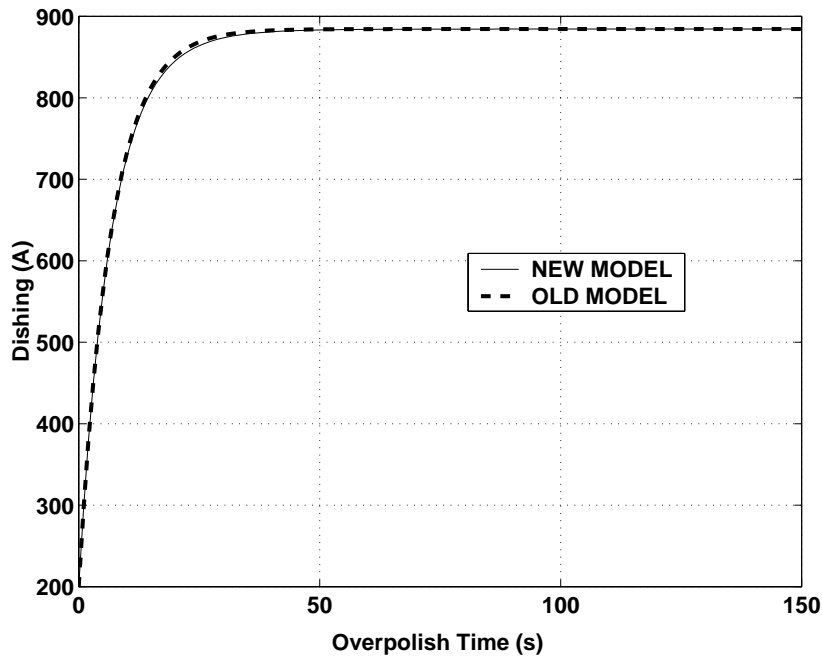
Recess and Step-Height versus time for 50  $\mu\text{m}$  width and space



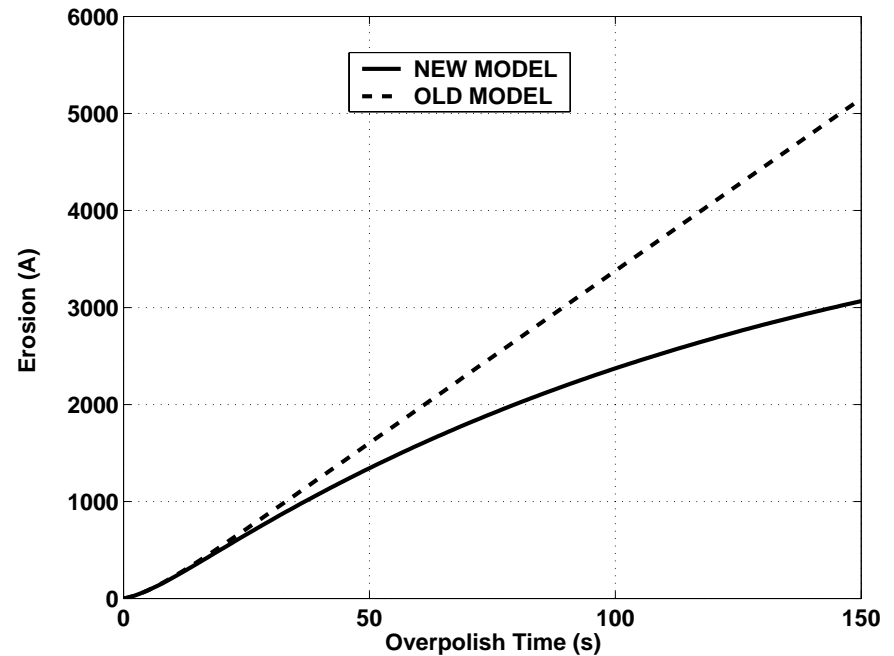
Recess and Step-Height versus time for 9  $\mu\text{m}$  width, and 1  $\mu\text{m}$  space

- The new model captures the recess and step-height trends

# Results: Stage 3 (Over-Polish)



Dishing versus polish time

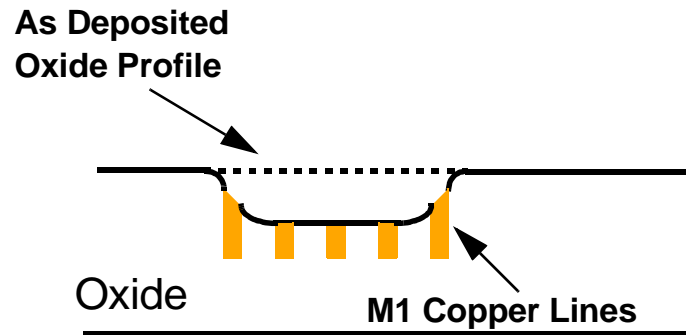


Erosion versus polish time

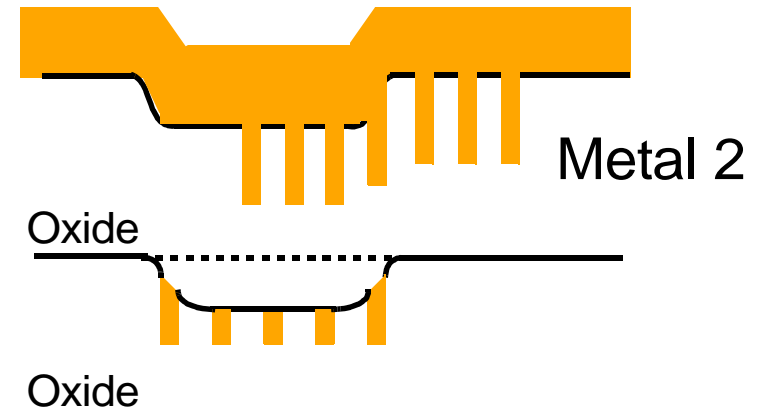
- Model captures the “reported” saturation of array erosion with excessive overpolish (array structure is surrounded by large field region).



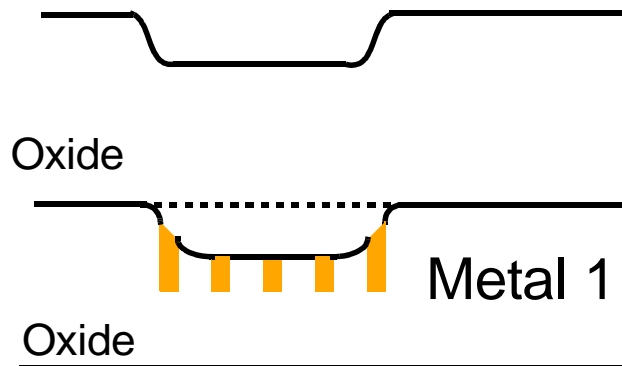
# 7. Multi-Level Copper Process Sequence



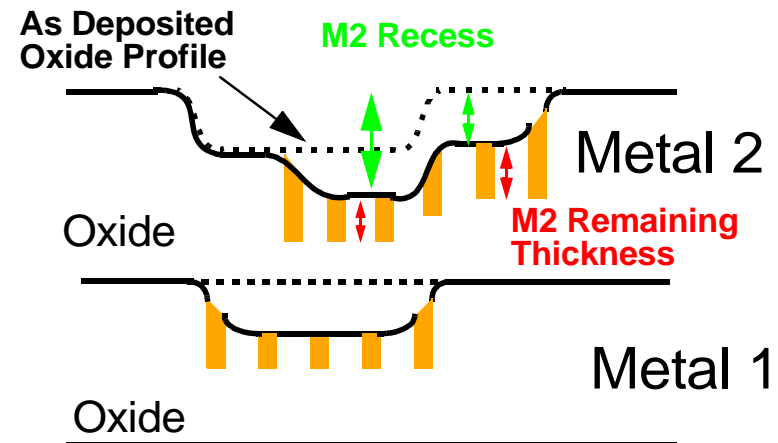
1. M1 Polish



3. M2 Cu Deposition

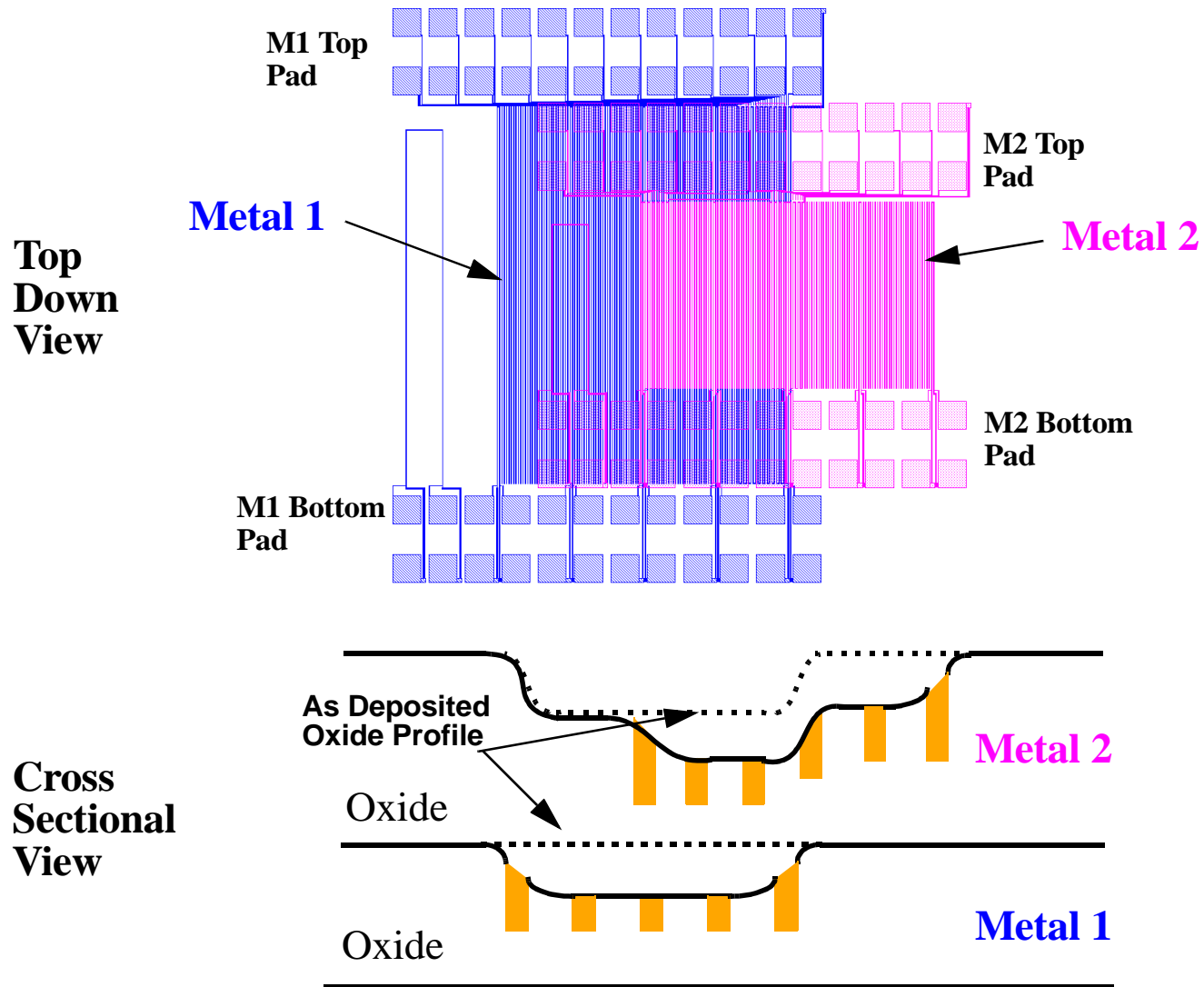


2. M2 Oxide Deposition



4. M2 Polish

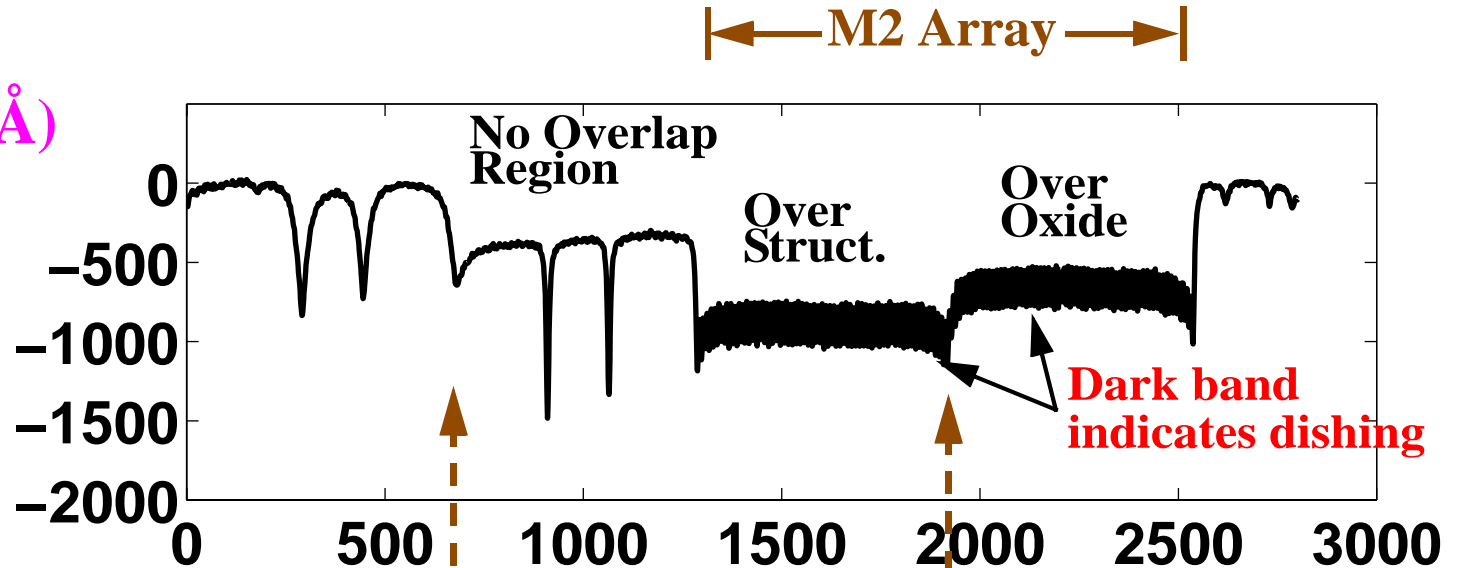
# Half Overlap Test Structure



# Half Overlap: Erosion to Dishing/Erosion

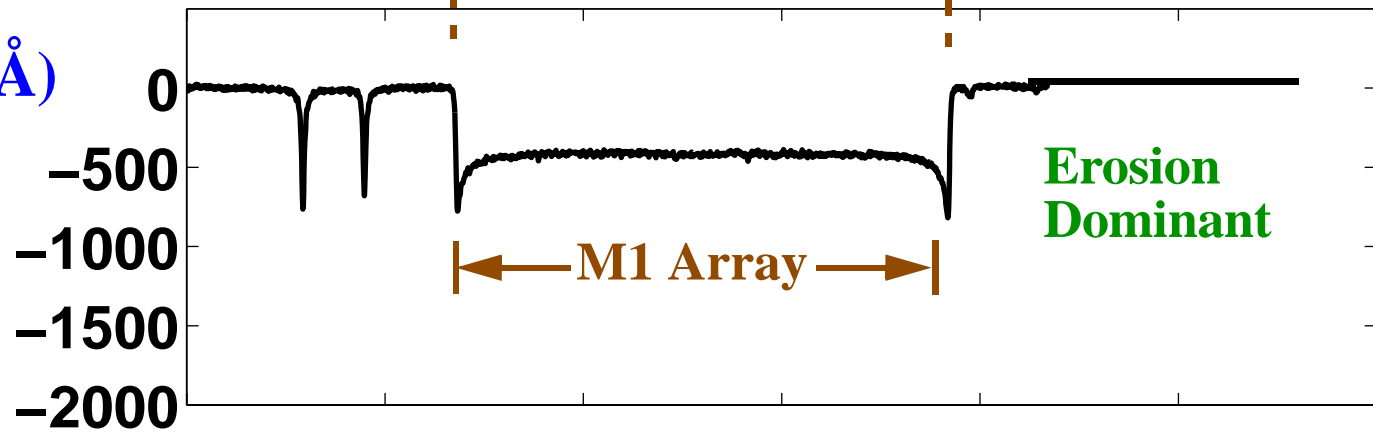
## M2 Profile (Å)

5 $\mu$ m Lw/  
5 $\mu$ m Ls



## M1 Profile (Å)

1 $\mu$ m Lw/  
1 $\mu$ m Ls



Scan Distance (μm)

# 8. Alternative Consumables Models: Fixed Abrasive Pad Effects

## ■ Conventional CMP:

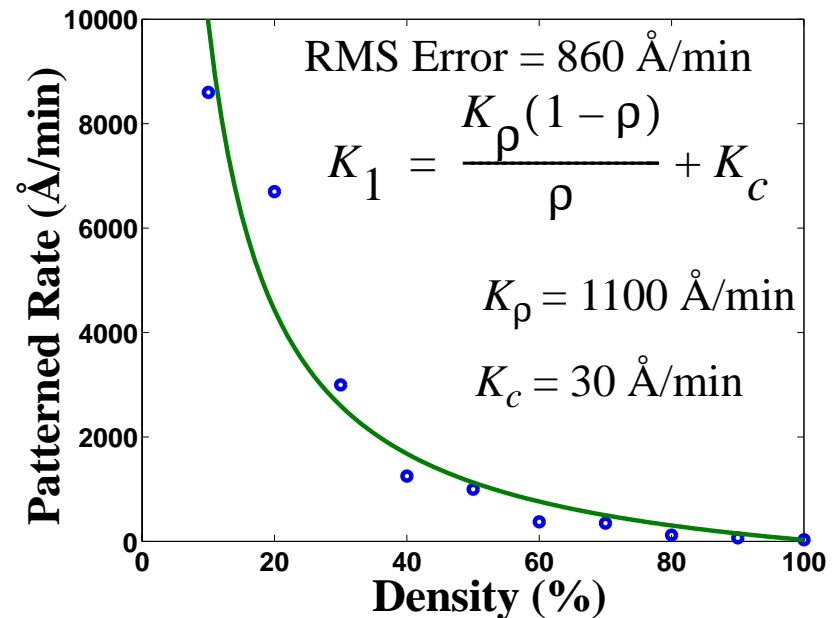
- ❑ Blanket polish rate:  
 $K \sim 1500 \text{ \AA/min}$
- ❑ Patterned polish rate:  
inversely proportional to  
pattern density  $\sim K/\rho$

## ■ Fixed Abrasive CMP:

- ❑ Low blanket polish rate:  
 $K_c \sim 30 \text{ \AA/min}$
- ❑ Patterned polish rate:  
much larger than  $K_c/\rho$ 
  - model patterned rate as

$$K_1 = \frac{K_\rho(1 - \rho)}{\rho} + K_c$$

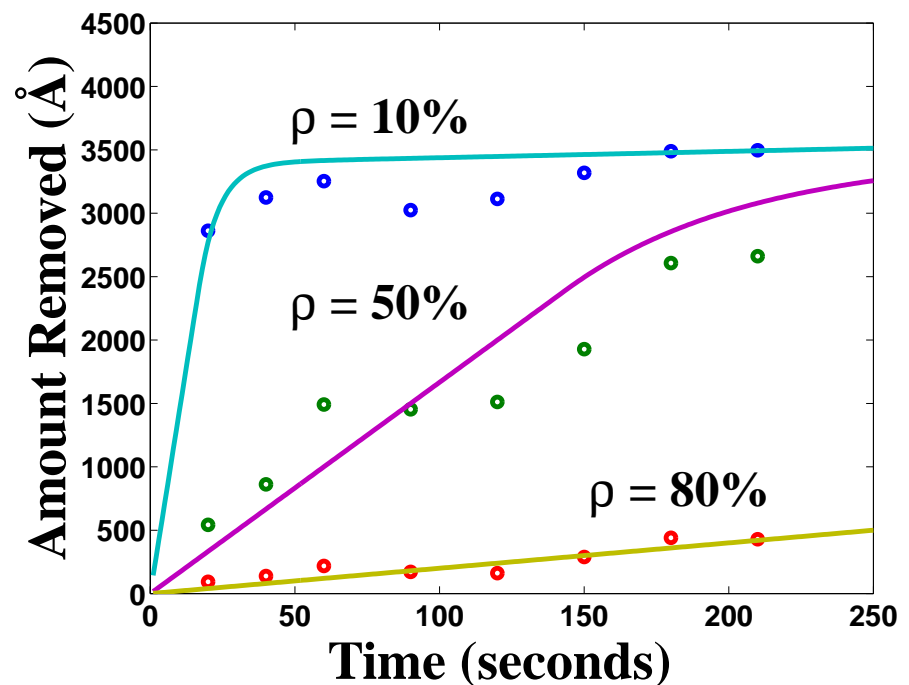
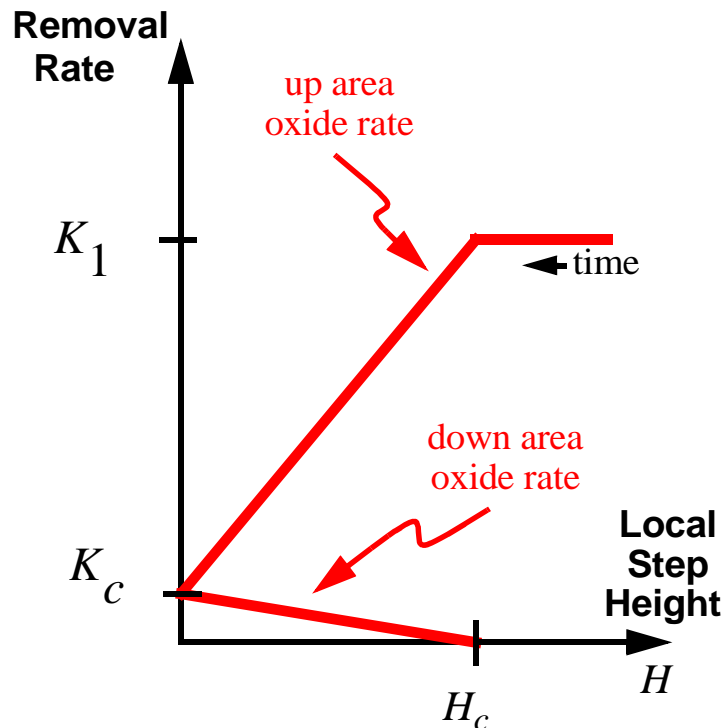
B. Lee et al., *CMPMIC 2001*



# Fixed Abrasive Pad CMP Model

- Decouple patterned rate from blanket rate:  $K_1 = \frac{K_p(1-\rho)}{\rho} + K_c$
- Apply density/step-height model with assumed linear rate dependence on step height between  $K_c$  and  $K_1$

Results:



# Status and Future Challenges in CMP Modeling

- Oxide (Interlevel Dielectric CMP)
  - ❑ Pattern density models are simple and provide good accuracy
  - ❑ Layout biasing for small linewidths accounts for deposition profile
  - ❑ Step height model for accurate up and down area predictions
- Shallow Trench Isolation CMP
  - ❑ Dual-material density/step-height models give reasonable accuracy for STI polishes with conventional consumables
  - ❑ Challenge: Nanotopography effects integrated with chip pattern effects
  - ❑ Challenge: Extended models to account for effects seen with new and alternative consumable sets (fixed abrasive pads, abrasive free slurry)
- Copper CMP
  - ❑ Challenge: calibration of models in realistic multi-step processes
  - ❑ Challenge: develop and integrate electrodeposition profile models
  - ❑ Challenge: multilevel CMP effects